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Heteroclinic and Compressible Fluids  
Heteroclinic Connection in Rapidly Rotating

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All these results were obtained for a Boussinesq fluid, but it is shown that a compressible layer exhibits analogous behaviour. As demonstrated by Jones et al. (1990), convection is necessarily unsteady and unsymmetric in this case but, as  $r$  is increased at sufficiently large horizontal boundary or the other.

The final summary of the paper includes some astrophysical calculations about the possibility bearing of this work on the regime of convection in the outer regions of the Sun.

Numerical solutions are presented for both these cases for several values of the Rayleigh number,  $r = \alpha B^2 / 2Uk$ , where  $\alpha$  is the coefficient of volume expansion,  $B$  is the applied adverse temperature gradient, and  $k$  is the thermal diffusivity. A symmetric-breaking bifurcation is located at large  $r$  in the case of stress-free side walls and sufficiently large For smaller  $r$  the solutions are steady and symmetric about the horizontal mid-level; for larger  $r$  they progress in opposite  $x$ -directions as horizontal waves hugging one horizontal boundary or the other.

For sufficiently large  $r$  the case of stress-free side walls and sufficiently large  $A$ , a symmetric-breaking bifurcation is located at large  $r$  in the case of stress-free side walls and sufficiently large  $A$ . All these results were obtained for a Boussinesq fluid, but it is shown that a compressible layer exhibits analogous behaviour. As demonstrated by Jones et al. (1990), convection is necessarily unsteady and unsymmetric in this case but, as  $r$  is increased at sufficiently large horizontal boundary or the other.

At the onset of convection in a stagnant layer, a Lorentz force,  $F$ , is created in the  $x$ -direction which, though weak, has a nonzero horizontal average that cannot be balanced by any other forces in the equation of motion. This force sets up a geostrophic flow,  $U$ , in the  $x$ -direction, i.e. a flow that depends on  $z$  alone. This flow affects  $F$ , and in a so-called "Tayler State" obliterates  $F$ . Such Tayler states are here shown to occur at small Froude numbers,  $A = \alpha B^2 / 2Uk$ , where  $\alpha$  is density,  $B$  is the electrical conductivity. At larger values of  $A$ , the amplitude of the geostrophic flow is determined by viscous friction, either at the vertical walls of the duct when these are rigid, or by viscous friction throughout the bulk of the fluid when the vertical walls are stress-free.

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Rapidly rotating magnetoconvection is believed to occur in the outer core of the Earth and in the convection zones of many stars. By rapidly rotating magnetoconvection, we mean that the Coriolis, Lorentz and buoyancy forces dominate the motions and are comparable in magnitude, so that the corresponding dimensionless measures of these forces, the Taylor, Chandrasekhar and Rayleigh numbers, are all large. The problem of under-standing the nature of convection in these circumstances is not a simple one, and in this paper were shall restrict our attention to some particular aspects.

The study of rapidly rotating magnetoconvection has close links, of both a mathematical and physical nature, with dynamics theory. It is widely believed that planetary and stellar magnetohydrodynamics could be obtained when the viscous terms were entirely omitted. This is an attractive feature as, in the applications of magnetohydrodynamics a certain restriction is too tiny to be significant, and the turbulent viscosity can only be crudely guessed. The philosophy generally adopted in numerical simulations (Gillman, 1983; Glatzmaier, 1984, 1985a, 1985b) is to select the smallest value of the viscosity for which numerical instabilities are absent. The viscosity of the Earth's core is generally believed to be small, although its actual value is uncertain to many orders of magnitude.

An issue that arises almost immediately is the role of viscosity. In the linear problem of marginal convection (El Tayeb, 1972), self-consistent solutions could be obtained when the viscous terms were omitted. This is an attractive feature as, in the applications of magnetohydrodynamics the viscosity is very uncertain, although almost certainly small. To the planets and stars, the viscosity is too tiny to be significant, and the turbulent viscosity can only be crudely guessed. The philosophy generally adopted in numerical simulations (Gillman, 1983; Glatzmaier, 1984, 1985a, 1985b) is to select the smallest value of the viscosity for which numerical instabilities are absent. The viscosity of the Earth's core is generally believed to be small, although its actual value is uncertain to many orders of magnitude.

We shall adopt a plane Cartesian geometry in this paper. Although all applications have the spherical geometry of naturally-occurring bodies, the use of a planar model greatly simplifies the mathematics, while still allowing us, we believe, to increase our understanding of the fundamental dynamics of rapidly rotating magnetoconvection in general geometries.

The study of rapidly rotating magnetoconvection from convection-drawn dynamos. A natural problem to the magnetic fields originate from convection-drawn dynamos. A natural problem to the study of the full dynamo problem is the analysis of convection in an imposed magnetic field, the magnetoconvection problem.

There are several ways of attacking magnetoconvection. One way is to consider the case of a rotating sphere with a uniform magnetic field. This is a simple problem, but it does not represent the Earth's magnetic field very well. Another way is to consider the case of a rotating sphere with a non-uniform magnetic field. This is a more difficult problem, but it represents the Earth's magnetic field much better. The third way is to consider the case of a rotating sphere with a complex magnetic field. This is a very difficult problem, but it represents the Earth's magnetic field very accurately.

The question arises, "Does a similar behavior occur in the magnetoconvection problem?" In general, the solutions of the linearized, convective instability problem do not seem? In fact, it has been considered by many authors, e.g. Zhang (1987), Zhang and Bussé (1988) and Meryhield (1990), and has also provided the basis for the simulations of solar convection by Gilman and Glatzmaier referred above. These authors find that convection induces a general differential rotation in their models, whereas only the geostrophic velocity and  $T$  is temperature, which is significant in our model; however, when  $T = O(1)$ , other nonlinearities, principally the advection of heat through the  $\nabla T$  term in the energy equation (where  $u$  is fluid velocity and  $T$  is temperature), occur simultaneously with the Ekman nonlinearity, so that in the rapidly rotating case, the feedback associated with the geostrophic wind occurs at the non-geostrophic part of the differential rotation as significant as the geostrophic part. In the rapidly rotating case, the feedback associated with the geostrophic wind occurs at the convectioning motion having the planform of undirectional rolls are possible, but are atypical combination of rolls in two different directions are present (and, in this geometry, such a Stewartsen model was studied further by Soward (1980, 1986), who confirmed their layer combination is typically the most relevant one), a geostrophic wind is set up. The Roberts-Stewartsen model was studied further by Soward (1980, 1986), who confirmed their layer horizontal by bounded vertical walls parallel to the applied field; in this duct model, the single roll planform of the unbounded layer is disallowed, and two roll systems are generally necessary. Soward showed that, for a wide range of parameters, the magnetic field moved towards a Taylor configuration at some second critical Rayleigh number,  $r_T$ . The Taylor's constraint was satisfied at some second critical Rayleigh number was increased, and that the single roll planform of the unbounded layer is disallowed, and two roll systems are also noted that, at small values of the ratio  $g = \kappa/\eta$  of magnetic to thermal diffusivities, the nature of the Taylor solution became rather complicated.

We should note that this type of nonlinearity is rather different from those normally associated with convecting systems. This is a consequence of assuming that the Taylor number,  $T$ , and the Chandrasekhar number,  $Q$ , are both large. The problem of slowly rotating magnetoconvection, where  $T$  and  $Q$  are of order 1 (or actually a few hundred, because of factors of  $u$ ) has been considered by many authors, e.g. Zhang (1987), Zhang and Bussé (1988) and Meryhield (1990), and has also provided the basis for the simulations of solar convection by Gilman and Glatzmaier referred above. These authors find that convection induces a general differential rotation in their models, whereas only the geostrophic velocity and  $T$  is temperature, which is significant in our model; however, when  $T = O(1)$ , other nonlinearities, principally the advection of heat through the  $\nabla T$  term in the energy equation (where  $u$  is fluid velocity and  $T$  is temperature), occur simultaneously with the Ekman nonlinearity, so that in the rapidly rotating case, the feedback associated with the geostrophic wind occurs at the non-geostrophic part of the differential rotation as significant as the geostrophic part. In the rapidly rotating case, the feedback associated with the geostrophic wind occurs at the convectioning motion having the planform of undirectional rolls are possible, but are atypical combination of rolls in two different directions are present (and, in this geometry, such a Stewartsen model was studied further by Soward (1980, 1986), who confirmed their layer combination is typically the most relevant one), a geostrophic wind is set up. The Roberts-Stewartsen model was studied further by Soward (1980, 1986), who confirmed their layer horizontal by bounded vertical walls parallel to the applied field; in this duct model, the single roll planform of the unbounded layer is disallowed, and two roll systems are generally necessary. Soward showed that, for a wide range of parameters, the magnetic field moved towards a Taylor configuration at some second critical Rayleigh number,  $r_T$ . The Taylor's constraint was satisfied at some second critical Rayleigh number was increased, and that the single roll planform of the unbounded layer is disallowed, and two roll systems are also noted that, at small values of the ratio  $g = \kappa/\eta$  of magnetic to thermal diffusivities, the nature of the Taylor solution became rather complicated.

The amplitude of the solution rapidly increased in magnitude, from a value of order  $E^{1/4}$ , where  $E$  is the Ekman number, to  $O(1)$ . If  $D$  is increased beyond  $D_T$ , meridional circulation terms become significant, and these new nonlinearities determine the amplitude in term? In general, the solutions of the linearized, convective instability problem do not seem? In fact, it has been considered by many authors, e.g. Zhang (1987), Zhang and Bussé (1988) and Meryhield (1990), and has also provided the basis for the simulations of solar convection by Gilman and Glatzmaier referred above. These authors find that convection induces a general differential rotation in their models, whereas only the geostrophic velocity and  $T$  is temperature, which is significant in our model; however, when  $T = O(1)$ , other nonlinearities, principally the advection of heat through the  $\nabla T$  term in the energy equation (where  $u$  is fluid velocity and  $T$  is temperature), occur simultaneously with the Ekman nonlinearity, so that in the rapidly rotating case, the feedback associated with the geostrophic wind occurs at the non-geostrophic part of the differential rotation as significant as the geostrophic part. In the rapidly rotating case, the feedback associated with the geostrophic wind occurs at the convectioning motion having the planform of undirectional rolls are possible, but are atypical combination of rolls in two different directions are present (and, in this geometry, such a Stewartsen model was studied further by Soward (1980, 1986), who confirmed their layer combination is typically the most relevant one), a geostrophic wind is set up. The Roberts-Stewartsen model was studied further by Soward (1980, 1986), who confirmed their layer horizontal by bounded vertical walls parallel to the applied field; in this duct model, the single roll planform of the unbounded layer is disallowed, and two roll systems are generally necessary. Soward showed that, for a wide range of parameters, the magnetic field moved towards a Taylor configuration at some second critical Rayleigh number,  $r_T$ . The Taylor's constraint was satisfied at some second critical Rayleigh number was increased, and that the single roll planform of the unbounded layer is disallowed, and two roll systems are also noted that, at small values of the ratio  $g = \kappa/\eta$  of magnetic to thermal diffusivities, the nature of the Taylor solution became rather complicated.

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$$B_0 = \frac{R(m+1)}{g}$$

where  $P_0$  is a constant pressure and

(2.7)

$$T_0 = B_0 z, \quad p_0 = P_0 \left( \frac{z}{z_m} \right)^{m+1}, \quad u_0 = 0, \quad B_0 = \text{const.}$$

Equations (2.1) - (2.6) admit the polytropic solution:

where  $T$  is temperature,  $p$  is pressure,  $u$  is fluid velocity, and  $B$  is magnetic field. The angular velocity  $\Omega$ , the acceleration due to gravity  $g$ , the gas constant  $R$ , the ratio of specific heats  $\gamma$ , the thermal conductivity  $K$ , the viscosity  $\mu$ , the magnetic diffusivity  $\eta$  and the magnetic permeability  $\mu_r$  are all assumed to be constant;  $\nu$  is the kinematic viscosity and  $\eta = 1/\mu\nu$ , where  $\alpha$  is the electrical conductivity. The coefficient of bulk viscosity is assumed to be zero.

(2.6)

$$\nabla \cdot B = 0,$$

(2.5)

$$p = R\rho T,$$

(2.4)

$$\frac{\partial p}{\partial t} \left( \frac{\partial T}{\partial t} + u \Delta T \right) = K \Delta^2 T + \frac{\rho}{\mu} \left( \frac{\partial p}{\partial t} + u \Delta p \right),$$

(2.3)

$$\frac{\partial B}{\partial t} = \Delta \times (u \times B - \eta \Delta \times B),$$

(2.2)

$$p \left( \frac{\partial u}{\partial t} + u \Delta u \right) + 2p \nabla \times u = -\Delta p + g p l_z + \frac{\mu}{1} (\Delta \times B) \times B + \rho u [\Delta^2 u + \frac{1}{3} \Delta (\Delta \cdot u)],$$

(2.1)

$$\frac{\partial \rho}{\partial t} + \Delta \cdot (\rho u) = 0,$$

The basic equations of this study are the continuity equation, the gas law, and the equation of motion, the electromagnetic induction equation, the energy equation, the gas law, and the equation that rules out magnetic monopoles:

## 2. BASIC EQUATIONS AND BOUNDARY CONDITIONS

Rayleigh number connects to a solution with convection occurring mainly in the tenuous zones, even in a homogeneous Boussinesq model. In the present nonlinear study, we find that the convective layer naturally divides into two regimes, unless one selects a two-layer model to represent the convection zone. Why there should be a separation of the convection zone into two independent convective zones, even in a homogeneous Boussinesq model, is hard to discern from linear theory. Any reason convection cells might be preferred. It is hard to discern from linear theory why there should be a separation of the convection zone into two independent convective zones, unless one selects a two-layer model to represent the convection zone. The local Elsasser number is small and Coriolis forces dominate Lorentz forces, "banana" zones, so favouring the formation of "doughnut" convection cells; at depth, however, where such a toroidal field may be expected to "channel" the fluid motion to be predominately toroidal, the local Elsasser number becomes large as the density falls near the solar surface, and the local Elsasser number is small and Coriolis forces dominate Lorentz forces, "banana" zones of some interest. It was conjectured in Paper I that the observations of Ribes et al (1985) might be explained as follows: the importance of the toroidal field, as measured by the top of the layer. This separation of the convection zone into two parts is of some interest. It was conjectured in Paper I that the observations of Ribes et al is of some interest. This separation of the convection zone into two parts region near the top of the layer. This separation of the convection zone into two parts region near the top of the layer. This separation of the convection zone into two parts

$$T_1 \leftarrow a [g^0 d(z_0 + \frac{z}{2})] T_1, \quad p_1 \leftarrow a \left[ \frac{p}{P} (z_0 + \frac{z}{2})^{m+1} \right] p_1, \quad p_1 \leftarrow a \left[ \frac{p}{P} (z_0 + \frac{z}{2})^{m+1} \right] p_1,$$

suggesting similar dimensionless groupings for  $T_1, p_1$  and  $p_1$ :

$$T_0 = [g^0 p(z_0 + \frac{z}{2})]^{\zeta}, \quad p_0 = \left[ \frac{p}{P} (z_0 + \frac{z}{2})^{m+1} \right]^{\zeta}, \quad \zeta = m + 1,$$

Then (2.7) gives

$$\zeta = z / (z_0 + \frac{z}{2}).$$

It is often convenient to relate variables to their values at the centre,  $z = z_0 + \frac{z}{2}$ , of the layer, and also to write

$$z_0 \leq z \leq 1 + z_0.$$

In these units the layer occupies the region

$$x \leftarrow dx, \quad t \leftarrow \frac{d}{\eta} t, \quad u \leftarrow \frac{d}{\eta} u, \quad B \leftarrow B^0 B. \quad (2.14)$$

We may carry out the process of thermodynamic linearization commonly called the anelastic approximation. As a first step, we transform to dimensionless variables by writing

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + u \Delta,$$

where  $D/Dt$  stands for the motional derivative:

$$\nabla \cdot B_1 = 0, \quad (2.13)$$

$$p_1 = R(T_0 p_1 + p_0 T_1 + p_1 T_1), \quad (2.12)$$

$$(p_0 + p_1) \left[ R \frac{DT_1}{Dt} + \frac{m+1}{9} u_z \right] = K \Delta^2 T_1 - (p_0 + p_1) \Delta \cdot u, \quad (2.11)$$

$$\frac{\partial B_1}{\partial t} = \Delta \times [u \times (B_0 + B_1) - \eta \Delta \times B_1], \quad (2.10)$$

$$+ \rho u [\Delta^2 u + \frac{3}{4} \Delta \cdot \nabla u], \quad (2.9)$$

$$(p_0 + p_1) \left[ \frac{Du}{Dt} + 2 \nabla \times u \right] = -\Delta p_1 + g p_1 I_z + \frac{\mu}{L} (\Delta \times B_1) \times (B_0 + B_1)$$

$$\frac{\partial p_1}{\partial t} + \Delta \cdot (p_0 u) + \Delta \cdot (p_1 u) = 0, \quad (2.8)$$

and similarly for other variables. Substitute into (2.1) - (2.6) to obtain

$$T = T_0 + T_1,$$

We now consider a convective state in which

is the temperature gradient. The fluid is confined to a horizontal layer of depth  $d$ .

$$a \leftarrow 0. \quad (2.21)$$

The anelastic approximation consists in taking the limit in which the superadiabatic gradient,  $\beta$ , is small compared with the total gradient,  $\beta_0$ ; since  $\beta/\beta_0 = \alpha\gamma(z_0 + \frac{1}{2})$  and since  $r$ ,  $g$  and  $z_0 + \frac{1}{2}$  are all  $O(1)$  quantities, this is tantamount to taking the limit and dimensionless measure of the buoyancy force.]

where  $\alpha$  is the coefficient of volume expansion; we therefore use a different letter,  $r$  for our velocity introduced in (2.14). The Rayleigh number is often taken to be  $\alpha\beta d^4/Uk$ , a dimensionless measure of a typical fluid velocity  $U$ . Here  $U$  is replaced by the unit  $g = \kappa/\eta$  is a ratio of diffusivities. [Usually the Rossby number is defined as  $U/2\alpha d$ ,

$$\rho_m = \frac{\rho d}{\rho(m+1)} (z_0 + \frac{1}{2})^m, \quad \beta = \beta_0 \left( \frac{\gamma(z_0 + \frac{1}{2})}{m+1} \right)^m K,$$

and  $\mathbf{I}_a$  and  $\mathbf{I}_b$  are unit vectors in the directions of  $\mathbf{U}$  and  $\mathbf{B}_0$ ,  $p_m$  is the density at the centre of the layer,  $\kappa$  is the thermal diffusivity at the centre of the layer, and  $\beta$  is the superadiabatic temperature gradient;

$$E = \frac{\rho u}{2\alpha d^2 p_m}, \quad Ro = \frac{\eta}{2\alpha d^2}, \quad A = \frac{B_0^2}{2\alpha p_m \eta \gamma}, \quad r = \frac{2\alpha p_m \eta \gamma}{g \beta d} (z_0 + \frac{1}{2}),$$

where  $E$ ,  $Ro$ ,  $A$  and  $r$  are Ekman, Rossby, Elsasser and Rayleigh numbers:

$$\Delta \cdot \mathbf{B}_1 = 0, \quad (2.20)$$

$$p_1 = \zeta_m T_1 + \zeta p_1 + \alpha p_1 T_1, \quad (2.19)$$

$$\frac{1}{\alpha} \frac{d\zeta_m + \alpha p_1}{dt} = \frac{q\gamma}{(\gamma-1)} \frac{(\zeta + \alpha T_1) D p_1}{D t} - \left[ \frac{q\gamma(z_0 + \frac{1}{2})}{1} \{ p_1 - m(\gamma-1)\zeta_{m-1} T_1 \} u_z + \Delta^2 T_1 \right], \quad (2.18)$$

$$\frac{\partial \mathbf{B}_1}{\partial t} = \nabla \times [\mathbf{u} \times (\mathbf{I}_b + \mathbf{B}_1) - \nabla \times \mathbf{B}_1], \quad (2.17)$$

$$+ E [\Delta^2 \mathbf{u} + \frac{3}{2} \Delta (\nabla \cdot \mathbf{u})], \quad (2.16)$$

$$(\zeta_m + \alpha p_1) \left[ Ro \frac{D \mathbf{u}}{Dt} + \mathbf{I}_a \times \mathbf{u} \right] = - \frac{m+1}{(z_0 + \frac{1}{2})} \Delta p_1 + p_1 \mathbf{I}_z + A (\nabla \times \mathbf{B}_1) \times (\mathbf{I}_b + \mathbf{B}_1) \quad (2.15)$$

Equations (2.8) - (2.13) may now be written as

$$a = \frac{g d}{2 \alpha \eta}.$$

where

$$\Delta \cdot B = 0. \quad (2.35)$$

$$\frac{d}{dT} = \Delta^2 T - ru_z, \quad (2.34)$$

$$\frac{\partial B}{\partial t} = \Delta \times [u \times (I_B + B) - \Delta \times B], \quad (2.33)$$

$$I_a \times u = -\Delta p + T z + A(\Delta \times B) \times (I_B + B) + E \Delta^2 u, \quad (2.32)$$

$$\Delta \cdot u = 0, \quad (2.31)$$

under which equations (2.23) - (2.28) simplify further to

$$z_0 \rightarrow \infty,$$

A large part of this paper will be devoted to the Boussinesq limit.

In these layers, the solution matches the mainstream to wall conditions. In the limit (2.30), but in which viscous forces are important even at leading order. In the limit (2.30), but in which viscous forces at the walls, whose thicknesses vanish in the limit (2.30), but in which (and this is essential) follows what follows in §3 onwards)  $E$  enters at higher orders, and boundary layers at the walls, whose thicknesses lead in order in the limit (2.30), but in which (and this is essential) follows what follows in §3 The solution can then usually be thought of as a "mainstream", in which (2.29) holds to

$$E \rightarrow 0. \quad (2.30)$$

We suppose instead that

$$E = 0. \quad (2.29)$$

that

Equations (2.23) - (2.28) are the basic starting point of this study. They are closely related to those on which Paper I was based. There are however two differences. First, we are interested here in the nonlinear developments of Paper I. We have therefore retained all nonlinear terms apart from those that were removed by (2.22) and the anelastic approximation (2.21). Second, we will retain the viscous term in (2.24). In Paper I, we assumed that

The solution can then usually be thought of as a "mainstream", in which (2.29) holds to

We are able here and below to omit the suffix  $I$ , without causing confusion.

$$\Delta \cdot B = 0. \quad (2.28)$$

$$p = \zeta_m T + \zeta_p, \quad (2.27)$$

$$\zeta_m \frac{d}{dT} = \frac{q\gamma}{(\gamma-1)} \zeta \frac{dp}{dt} - \left[ r \zeta_m + \frac{q(z_0 + \frac{z}{l})}{l} \right] \{ p - m(\gamma-1) \zeta_{m-1} T \} u_z + \Delta^2 T, \quad (2.26)$$

$$\frac{\partial B}{\partial t} = \Delta \times [u \times (I_B + B) - \Delta \times B], \quad (2.25)$$

$$\zeta_m I_a \times u = -\frac{m+\frac{1}{2}}{(z_0 + \frac{z}{l})} \Delta p + p I_z + A(\Delta \times B) \times (I_B + B) + E [\Delta^2 u + \frac{1}{l} \Delta (\Delta \cdot u)], \quad (2.24)$$

$$\Delta \cdot (\zeta_m u) = 0, \quad (2.23)$$

Equations (2.15) - (2.20) then become

$$Ro \rightarrow 0. \quad (2.22)$$

In addition we shall confine attention to vanishing Rossby numbers

This is because we have yet to impose the condition that no sources of field exist in the insulator (except for the current sources that create  $B_0$ ). When we add this demand, evidently (2.37p) place two restrictions on the solution, but apparently (2.37i) places three.

$$\text{insulator: } \langle B_z \rangle = \left( \frac{\partial B_z}{\partial z} \right) = j_z = 0, \text{ at } z = z_0, l + z_0, \quad (2.37i)$$

$$\text{perfect conductor: } B_z = \frac{\partial j_z}{\partial z} = 0, \text{ at } z = z_0, l + z_0, \quad (2.37p)$$

we see that

$$\mathbf{j} = \nabla \times \mathbf{B},$$

Using (2.6) we see that only two of these three conditions are independent. Introducing the (dimensionless) electric current density  $\mathbf{j}$ , by

$$\frac{\partial B_z}{\partial z} = \frac{\partial B_y}{\partial z} = B_z = 0,$$

so that at a perfectly conducting boundary

$$\mathbf{E} = -\mathbf{u} \times \mathbf{B} + \eta \nabla \times \mathbf{B},$$

is the vorticity. The magnetic conditions depend on the electrical properties (and extent) of the regions  $z < z_0$  and  $z > l + z_0$ . We shall consider only the two extreme cases in which these regions are perfect electrical insulators or are perfect electrical conductors. In the former case all conditions are satisfied by making  $\mathbf{B}$  continuous; in the latter case no  $\mathbf{B}$  and  $\mathbf{n} \times \mathbf{E}$  must vanish at a wall, where  $\mathbf{n}$  is the normal to the wall and  $\mathbf{E}$  is the electric field: in dimensional units

$$\omega = \nabla \times \mathbf{u}$$

where

$$\text{stress-free: } u_z = \frac{\partial^2}{\partial z^2} (\zeta_m u_z) = 0, \text{ at } z = z_0, l + z_0, \quad (2.36f)$$

$$\text{no-slip: } u_z = \frac{\partial u_z}{\partial z} = \omega_z = 0, \text{ at } z = z_0, l + z_0, \quad (2.36r)$$

We shall find it more convenient to use the equivalent demands

$$\text{stress-free: } \frac{\partial u_x}{\partial z} = \frac{\partial u_y}{\partial z} = u_z = 0.$$

$$\text{no-slip: } u_x = u_y = u_z = 0,$$

The basic equations (2.23) - (2.28) or (2.31) - (2.35) are of twelfth order, and six boundary conditions are required at each of the horizontal boundaries. These conditions are mechanical, magnetic and thermal. The surfaces may be "rigid" or "free", which means that the mechanical conditions are of one of two types: no-slip or stress-free:

which were used exclusively in paper I.

$$T = u_z = B_z = 0, \quad \text{at } z = z_0, l + z_0, \quad (2.42)$$

except in parts of §§3 and 5, we shall no longer employ Elsayeb's (1972) illustrative conditions

$$\text{insulator: } \frac{\partial B_z}{\partial z} \mp \sqrt{(k^2 + l^2)} B_z = T = 0, \quad \text{at } z = z_0 + \frac{l}{2} \mp \frac{1}{2}. \quad (2.41i)$$

$$\text{perfect cond.: } B_z = T = 0, \quad \text{at } z = z_0, l + z_0, \quad (2.41p)$$

where upper and lower signs are to be taken together. The mechanical conditions, whether boundary layers on  $z = z_0$  and  $z_0 + l$  are absorbed into the pressure gradient, and the theory of magnetohydrodynamic duct flow. Their thickness is  $M_{1/2}d$ , where  $M = B_0 d / \sqrt{\mu \rho_0 n_V}$  is the Hartmann number, whose square (the Chandrasekhar number) measures the relative strength of Lorentz and viscous forces. From the theory of these layers, it emerges that the mainstream is required to obey

$$\text{insulator: } J_z = \frac{\partial B_z}{\partial z} \mp \sqrt{(k^2 + l^2)} B_z = T = 0, \quad \text{at } z = z_0 + \frac{l}{2} \mp \frac{1}{2}, \quad (2.40i)$$

$$\text{perfect cond.: } B_z = \frac{\partial J_z}{\partial z} \pm (k \operatorname{sgn} l) u_z = T = 0, \quad \text{at } z = z_0 + \frac{l}{2} \mp \frac{1}{2}; \quad (2.40p)$$

the case we shall consider below, conditions (2.36) - (2.38) require that the mainstream solutions obey

$$\exp[i(kx + ly + wt)], \quad (2.39)$$

Following the geometry of paper I, in which  $J$  and  $B$  are horizontal and perpendicular to one another, we shall take  $J_B = J_x$  and  $J_A = J_y$ . In the limit (2.30), the mainstream is governed by the  $E = 0$  forms of (2.23) - (2.28) or (2.31) - (2.35), which are then capable of satisfying only three conditions at each of the horizontal walls ( $l \neq 0$ ) or two systems of only sixth order ( $l \neq 0$ ) or fourth order ( $l = 0$ ). The mainstream is therefore considered to be of satisfying only six conditions being met by boundary layers. For ( $l \neq 0$ ), the remaining conditions being met by boundary layers. For ( $l \neq 0$ ), the analysis of these "side-wall" layers (so-called because in the theory of rotating fluids  $J$  is often regarded as being "vertical") has been undertaken by Condi (1978); see also Fearns (1983). We state here only the final result of his analysis. In the case in which solutions are proportional to

$$T = 0, \quad \text{at } z = z_0, l + z_0. \quad (2.38)$$

We shall make the usual assumption, that the walls are perfect thermal conductors, so that the thermal conditions, which also depend on the nature of the containing walls, consider the thermal conditions on the solution. Finally we shall find that (2.36i) also embodies only two restrictions on the solution.

the walls. This is however not true of finite amplitude, or of non-Boussinesq convection. The results of linear Boussinesq theory are independent of the conditions placed on  $B_z$  on the onset of convection, and  $B_z$  can be determined later (if desired). In this restricted sense, the factor out from the fourth-order system determining  $u_z$  and  $T$ , i.e. the latter determining  $B_z$ , rather than one of the physically-motivated conditions (2.40). It transpires however that, in the linear Boussinesq theory that follows, the equation and boundary condition determine  $B_z$  rather than  $T$ .

$$T = u_z = B_z = 0, \quad \text{at } z = 0, 1, \quad (3.8)$$

In paper I, we assumed for simplicity the simple boundary conditions (2.42): We have omitted the viscous term in (3.4), i.e. (3.3) - (3.7) govern the mainstream solution.

$$\Delta \cdot B = 0. \quad (3.7)$$

$$\frac{\partial}{\partial T} = \Delta^2 T - ru_z, \quad (3.6)$$

$$\frac{\partial B}{\partial t} = \Delta \times [u \times (I_B + B) - \nabla \times B], \quad (3.5)$$

$$I_B \times u = -\Delta p + T T_z + A (\Delta \times B) \times (I_B + B), \quad (3.4)$$

$$\Delta \cdot u = 0, \quad (3.3)$$

Departures from state (3.2) are governed by (2.31) - (2.35): where  $a_0$  is the coefficient of volume expansion.

$$E = \frac{v}{2Ud^2}, \quad R_o = \frac{\eta}{2Ud^2}, \quad A = \frac{2U_p a_0}{B_o^2}, \quad r = \frac{g a_0 B_o^2 d}{2U_k},$$

(where, for consistency with the compressible case,  $z = 0$  is the top of the layer) and  $E$ ,  $R_o$ ,  $A$  and  $r$  reduce to

$$0 \leq z \leq 1,$$

We may now take the layer to be

$$T_0 = z, \quad p_0 = z - \frac{1}{2} z^2 + \text{const.}, \quad p_0 = \text{const.}, \quad u_0 = 0, \quad B_0 = I_z. \quad (3.2)$$

or in dimensionless units

$$T_0 = g z, \quad p_0 = g p_0 (z - \frac{1}{2} a_0 B_z^2) + \text{const.}, \quad p_0 = \text{const.}, \quad u_0 = 0, \quad B_0 = \text{const.} \quad (3.1)$$

In this and subsequent sections, we consider only the Boussinesq limit; compressibility will be reinstated in §7. The basic conduction solution replacing (2.7) is

### 3. SMALL AMPLITUDE BOUSSINESQ SOLUTIONS

Finally, we shall later (for reasons given in §3) limit our system horizontally, by plane vertical walls at  $y = \pm \frac{1}{2} L$ . The boundary conditions to be applied at these walls will be discussed in §§4 and 5.

$$(4A^2 - 1)(X^2 - A^2) + (A^2 + 1)X - 1 = 0,$$

where  $X (< \frac{1}{2})$  is the larger of the two positive roots of

$$k_c = \pm \sqrt{\left(\frac{X(1-2X)}{X^2}\right)}, \quad l_c = \pm \sqrt{\left(\frac{1-X}{1+X}\right)}, \quad r_c = \frac{1-X}{X} \sqrt{\left(\frac{1-X}{1+X}\right)}, \quad (3.17a)$$

If  $A > 4$ , there are two convective rolls, equally inclined to both  $\mathbf{U}$  and  $\mathbf{B}_0$ , which are the first to connect when, starting from state (3.2),  $r$  is increased from zero:

$$k_c \rightarrow 0, \quad l_c \equiv 0, \quad r_c = \pi^2 A.$$

of indefinitely large  $x$ -dimension:

If  $A < 4$ , the critical mode is a single convection roll parallel to the rotation axis and the tilde and the prime will be omitted from  $T^*$ , etc. Where possible,  $\mathbf{u}$ , and  $\mathbf{B}'$ , are complex, and their conjugates will be denoted by  $\tilde{\mathbf{T}}^*$ , etc. The functions  $T^*$ ,  $\tilde{\mathbf{u}}$ , and  $\mathbf{B}'$ , are the one that minimizes  $r_m$  over  $k$  and  $l$ . [The functions  $T^*$ ,  $\tilde{\mathbf{u}}$ , and  $\mathbf{B}'$ , are complex, and their conjugates will be denoted by  $\tilde{T}^*$ , etc. Where possible,  $\tilde{\mathbf{u}}$ , and  $\mathbf{B}'$ , are the one that minimizes  $r_m$  over  $k$  and  $l$ .] The critical state ( $r_m = r_c$ ) is direct

$$r_m = \frac{l^2(k^2 + l^2 + \pi^2)^2}{Ak^2(k^2 + l^2)} + \frac{Ak^2(k^2 + l^2 + \pi^2)}{k^2 + l^2}. \quad (3.16)$$

where  $c.c.$  stands for the complex conjugate, the marginal state ( $r = r_m$ ) is direct

$$T^*(x, y, z, t) = T^*(z) \exp[i(kx + ly + wt)] + c.c., \quad (3.15)$$

Paper I. It is there shown that, for solutions depending on  $x$ ,  $y$  and  $t$  as in (2.39), i.e. The solution to (3.8) and (3.10) - (3.14) may be found in Eltayeb (1972) or in §4 of

$$\nabla \cdot \mathbf{B}' = 0. \quad (3.14)$$

$$\frac{\partial}{\partial t} = \Delta^2 T' - ru_z, \quad (3.13)$$

$$\frac{\partial \mathbf{B}'}{\partial t} = \Delta \times (\mathbf{u} \times \mathbf{l}^z) + \Delta^2 \mathbf{B}', \quad (3.12)$$

$$\mathbf{l}^z \times \mathbf{u} = -\Delta p' + T'^z + A(\Delta \times \mathbf{B}') \times \mathbf{l}^z, \quad (3.11)$$

$$\Delta \cdot \mathbf{u} = 0, \quad (3.10)$$

products of the primed variables, to obtain a set of linear equations: and similarly for other variables. Substitute into (3.3) - (3.7), and neglect squares and

$$T = z + T^*, \quad (3.9)$$

The linear stability of state (3.2) is examined by writing

$$\frac{d}{dz} \left( B_z \frac{dB_z}{dz} - B_z^* \frac{dB_z^*}{dz} \right) = 0, \quad (3.24)$$

$$\frac{dp}{dz} (u_z B_z^* - u_z^* B_z) = 0, \quad (3.23)$$

We might intuitively expect that, for the ultimate equilibrium  $\mathbf{U}(z)$ , the force  $\mathbf{F}(z)$  will vanish, and this suggests a definite numerical procedure: iterate on  $\mathbf{U}(z)$  until  $\mathbf{F}(z) = 0$ , i.e. until, in terms of the representation (3.15),

$$\frac{g}{\rho T'} + \mathbf{U} \cdot \nabla T' = \Delta^2 T' - r u_z. \quad (3.22)$$

$$\frac{\partial \mathbf{B}'}{\partial t} + \mathbf{U} \cdot \nabla \mathbf{B}' = \nabla \times (\mathbf{u} \times \mathbf{l}') + \Delta^2 \mathbf{B}', \quad (3.21)$$

This type of difficulty was first described by Taylor (1963) in the context of geodynamics theory. It was encountered first in the theory of magnetoconvection by Roberts and Stewartsen (1975); see also Soward (1980). The weak horizontal force (3.20) is independent of  $x$  and  $y$ , and this suggests that it will, acting over a sufficiently long time (dependent on the amplitude of the force, i.e. on the degree of supercriticality), set up a horizontal motion independent of  $x$  and  $y$ . This geostrophic velocity shear will affect the convective motions; in other words, its presence invalidates the formulation (3.10) – (3.14) of the linear stability problem. In particular, (3.11) and (3.12) should be replaced by

is nonzero for all  $A$  [even when single rolls with ( $t \neq 0$ ) are excited], but there is no other term in (3.4), that can balance this force!

$$\mathbf{F}(z) = A [\Delta \times \mathbf{B}'] \times \mathbf{B}'^H, \quad (3.20)$$

which appears in the equation of motion (3.4) from the set (3.3) – (3.8) determining the „variables. The horizontal part (denoted by the suffix  $H$ ) of the horizontal average (denoted by an overbar) of (3.19),

$$A(\Delta \times \mathbf{B}') \times \mathbf{B}', \quad (3.19)$$

and similarly for the other variables. In the present problem, it is not at once apparent how the dynamical balance is achieved in this state. A difficulty arises from the term, solutions to (3.3) – (3.8):

If, holding  $k$  and  $t$  fixed, one increases  $r$  slightly beyond  $r_m$ , the convective state acquires a small but finite amplitude, which can be determined by a so-called „weakly nonlinear analysis”, in which (3.9) is taken to be the first two terms in an amplitude expansion of

$$A = \frac{1-x}{1+x} \sqrt{\left( \frac{x}{1+x} \right)}. \quad (3.17b)$$

i.e.

$$T_r(x, y, z, t) = T_r(z) \exp[i(kx + wt)] \cos ly + c.c., \quad (3.30)$$

The case when two rolls of the form (3.15) are simultaneously present, one with  $k_l > 0$  the other with  $k_l < 0$ , is more intricate. We shall suppose that these two rolls are excited to equal amplitude, a case relevant to the duct models of §§4-6. Then (3.15) is replaced by from which it also follows that  $u_z \equiv 0$ .

$$\beta \equiv 0, \quad i.e. \quad B_z \equiv 0,$$

It follows that

$$\int_1^0 \left( d\beta \right)^2 \left[ k_z^2 + l_z^2 + \left( \frac{dp}{d\phi} \right)^2 \right] + \left( \frac{zp}{d\phi} \right)^2 dz = 0. \quad (3.29)$$

Multiplying through by  $\beta$ , integrating across the layer, and making use of the fact that, by (3.8),  $\beta = 0$  on the walls, we obtain

$$\frac{d^2\beta}{dz^2} - \left[ k_z^2 + l_z^2 + \left( \frac{dp}{d\phi} \right)^2 \right] \beta = 0. \quad (3.28)$$

On substituting (3.26) into the  $z$ -component of the induction equation (3.21), multiplying by  $\exp(-i\phi)$ , and making use of (3.27), we obtain

$$\theta \equiv \phi + nl, \quad (3.27)$$

so that, either  $a \equiv 0$  or  $\beta \equiv 0$ , or (as we shall now suppose) for some integer  $n$ ,

$$a\beta \sin(\theta - \phi) = 0, \quad \text{for all } z,$$

where  $a$ ,  $\beta$ ,  $\theta$ , and  $\phi$  are real functions. Then (3.25) gives

$$u_z(z) = a(z) e^{i\theta(z)}, \quad B_z(z) = \beta(z) e^{i\phi(z)}, \quad (3.26)$$

Introduce the polar representation,

$$u_z(z) B_z^*(z) - u_z^*(z) B_z(z) = 0. \quad (3.25)$$

We shall now show by a reduction ad absurdum argument that, when convection occurs as the single roll (3.15), a Taylor state is impossible. Suppose a Taylor state exists, so that (3.23) holds. On integrating, using (3.8), we see that and terminology of Braginsky (1975), also made in the context of geodynamo theory.

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When such a solution can be found, it is appropriate to call it a Taylor State, since as envisaged by Taylor (1963) it resolves the dilemma of the unbalanced force,  $F(z)$ , without invoking coupling to the walls (e.g. without introducing viscous friction). If, however, a solution can be found only when some form of coupling is restored (in our case viscous friction), it would be appropriate to describe it as of Model-Z form, following the suggestion of Braginsky (1975), also made in the context of geodynamo theory.

$$k_6 A^2 \leq 4l^4 (u^2 + k^2 + l^2). \quad (3.38)$$

The integrand in (3.37) is non-negative for all  $d\phi/dz$  if

$$\int_1^0 [ \left( \frac{zp}{\phi p} \right)^2 + \left( \frac{zp}{\phi p} \right) \frac{l^2}{k^2 A} ] dz \geq 0. \quad (3.37)$$

so that by (3.35)

$$\int_1^0 z^2 \leq z p \left( \frac{dp}{d\phi} \right)^2 dz, \quad (3.36)$$

Since  $\phi = 0$  at  $x = 0$  and 1, a variational inequality gives

$$\int_1^0 \left( \frac{dp}{d\phi} \right)^2 dz + \left[ \left( \frac{zp}{\phi p} \right)^2 + \left( \frac{zp}{\phi p} \right) \frac{d}{dz} \left( \frac{dp}{d\phi} \right) \right] dz = 0. \quad (3.35)$$

Using again the polar representation (3.26) and integrating (3.33) across the layer, making use of the fact that, by (3.8),  $\phi = 0$  on the walls, we obtain in place of (3.29)

$$\begin{aligned} & \left( \frac{B_z}{k^2 A} \frac{dB_z}{dz} - B_z^* \frac{dB_z^*}{dz} \right) = \\ & \left[ \frac{dz}{p} \left( B_z^* \frac{dB_z}{dz} \right) - 2 \left( \frac{dz}{p} \right) \frac{dB_z}{dz} + (k^2 + l^2) B_z B_z^* \right] \end{aligned} \quad (3.34)$$

Now suppose that a Taylor state exists, and use (3.32) to rewrite the right-hand side of (3.33), so obtaining

$$B_z \frac{dB_z}{dz} + B_z^* \frac{dB_z^*}{dz} - 2(k^2 + l^2) B_z B_z^* = -ik(u_z B_z^* - u_z^* B_z). \quad (3.33)$$

Multiplying the  $z$  component of the induction equation (3.21) by  $B_z^*$  and taking the real part, we find that

$$(u_z B_z^* - u_z^* B_z) + \frac{k^2 A}{l^2} \left( B_z \frac{dB_z}{dz} - B_z^* \frac{dz}{p} \right) = 0. \quad (3.32)$$

When boundary conditions (3.8) apply, (3.31) may be integrated to give

$$\frac{dz}{p} \left\{ (u_z B_z^* - u_z^* B_z) + \frac{k^2 A}{l^2} \left( B_z \frac{dB_z}{dz} - B_z^* \frac{dz}{p} \right) \right\} = 0. \quad (3.31)$$

Taylor state is decided by whether or not  $U_z$  can be found such that  $F_z = 0$ . This requires  $u_y, w_z, B_z, B_z^*,$  and  $f_z$ . In this case  $F_y \equiv 0$  and therefore  $U_y \equiv 0$ ; the existence of a similarily for  $u_z$  and  $B_z^*$  is given in place of  $cos^2 y$  in the representations of  $u_x$ ,

$$+ \nabla(k^2 + l^2)[\theta_2(0) + \theta_2(1)] = 0. \quad (3.43)$$

$$zp \left\{ \theta_2^2 \left[ \left( \frac{dz}{dp} \right)^2 + \left( \frac{dp}{dz} \right) \frac{l^2}{k^2 A} \right] + \left( \frac{dp}{dz} \right)^2 \right\} + \int_1^0 \left\{ \left( \frac{dp}{dz} \right)^2 \right\} dz = 0.$$

The impossibility of Taylor states is as obvious as before.  
Turning now to the double-roll case, (3.35) is replaced by

$$\int_1^0 \left\{ \left( \frac{dp}{dz} \right)^2 + \left[ k^2 + l^2 + \left( \frac{dp}{dz} \right)^2 \right] + \nabla(k^2 + l^2)[\theta_2(0) + \theta_2(1)] \right\} dz = 0. \quad (3.42)$$

Very similar conclusions may be drawn about the Taylor states when (3.41) apply. Consider first the case of the simple roll system. Equation (3.28) is again valid, but  $\theta$  no longer vanishes on the walls, so that in place of (3.29) we have

to replace the condition on  $\dot{\gamma}_z$  in (2.40i) by a like condition on  $u_z$ .

$$\frac{\partial \dot{\gamma}_z}{\partial z} = - \frac{1}{A} \frac{\partial \theta}{\partial u_z},$$

We have here used the  $z$ -component of the curl of (3.11), namely

$$T = u_z = \frac{\partial B_z}{\partial z} \mp \nabla(k^2 + l^2)B_z = 0, \text{ at } z = \frac{1}{2} \pm \frac{1}{2}. \quad (3.41)$$

conditions (2.40i) that apply when the walls  $z = 0, 1$  are insulating:  
In the main bulk of this paper we shall apply, not (3.8), but the physically more realistic conditions (2.40i) that such Taylor states will exist at values of  $A$  greater than 4.  
In the  $k$  and  $l$  of stable modes should be inserted into (3.38), and at large values of  $A$  it may happen that such Taylor states will exist at values of  $A$  greater than 4.  
only the  $k$  and  $l$  of stable finite amplitude mode at supercritical Rayleigh numbers. Ideally corresponds to a stable finite amplitude mode at large numbers. Ideally is by no means clear that the wavenumbers of the preferred mode at marginal stability will Taylor states, if they exist, are irrelevant. This inference may, however, be too simplistic. It is for the double rolls, that are preferred at marginal stability. This suggests that the roll, and not the double rolls, that are preferred at marginal stability. This single roll, and so far this value of  $A$  no Taylor state is possible. For this value of  $A$  it is the  $l = 0$  single roll, and not the double rolls, that are preferred at marginal stability. This suggests that the roll, and not the double rolls, that are preferred at marginal stability. This single roll, and so far this value of  $A$  no Taylor state is possible. For this value of  $A$  it is the  $l = 0$  single

$$A \geq 3.5035 \dots \quad (3.40)$$

so that (3.37) cannot be satisfied if

$$x \geq \frac{1}{4}(\sqrt{17} - 3),$$

or

$$2x^2 + 3x - 1 \geq 0, \quad (3.39)$$

Combining attention to the critical mode for which (3.17) holds, we may translate (3.38) into

so they do not define the critical Rayleigh number. The  $\lambda = 0$  linear solutions satisfy extenions appear as dashed curves in Figure 1; they lie above the solid curve, of course, comprise this stability boundary can be extended above and below  $A = 4$ , and these two curves which is why the solid curve has a discontinuity in slope at  $A = 4$ . The two curves is governed by the  $\lambda = 0$  mode, and for  $A > 4$  by modes with both  $k$  and  $\lambda$  non-zero; solid lines give the critical Rayleigh number at which convection onset: for  $A \leq 4$  this is as indicated in Figure 1, where the  $(A, \lambda)$ -plane for insulating walls is displayed. The indeed, our numerical scheme has found Taylor states for values of  $A$  below 4. The situation For values of  $A$  not satisfying inequality (3.51) Taylor states cannot be ruled out, and This is the replacement of (3.40) for insulating walls.

$$(3.51) \quad A \geq 4.080 \dots$$

so that no Taylor state can exist when

$$(3.50) \quad \lambda \geq 0.339 \dots$$

? From these relations it follows that

$$(3.49) \quad 2\lambda^3 + \left(1 + \frac{\pi^2}{4\lambda^2}\right)\lambda^2 + 2\lambda - 1 \geq 0.$$

$$(3.48) \quad \tan \lambda = \frac{\lambda^2 - \pi^2 \lambda}{2\pi \lambda^{1/2}}$$

Again confining attention to the critical wavenumbers (3.17), we may translate (3.45) and (3.47) into

$$(3.47) \quad k_6 A^2 \leq 4\lambda^4 (\lambda^2 + k_2^2 + l_2^2).$$

so that there are no Taylor states when

$$(3.46) \quad \int_1^0 \left[ \lambda^2 + k_2^2 + l_2^2 + \frac{k_6^2 A^2}{\lambda^2} \left( \frac{zp}{\phi p} \right)^2 + \left( \frac{zp}{\phi p} \right) \frac{l_2^2}{\lambda^2} \right] \beta_2^2 dz \leq 0,$$

Inequality (3.36) is now replaced by

$$(3.45) \quad \tan \lambda = \frac{\lambda^2 - k_2^2 - l_2^2}{2\lambda \sqrt{(k_2^2 + l_2^2)}}$$

where  $\lambda$  is the smallest positive root of

$$(3.44) \quad \int_1^0 \left[ \lambda^2 dz + \lambda^2 (k_2^2 + l_2^2) [\beta_2(0) + \beta_2(1)] \right] \geq \lambda^2 \int_1^0 \left( \frac{zp}{\phi p} \right)^2 \beta_2^2 dz,$$

The variational inequality appropriate to the boundary condition (3.41) is not (3.36) but

$(\nabla \times B') \times B'$ , can of course be balanced by a vertical pressure gradient. This equation is obtained from the geostrophic part of (2.32), i.e. its horizontal average. The remaining (non-geostrophic) part, of  $(\nabla \times B') \times B'$ , creates an order  $E$  velocity, which is negligible to the approximation to which we are working. The vertical component of  $(\nabla \times B') \times B'$

$$\Delta^2 U + A [\underline{(\nabla \times B') \times B'}] = 0. \quad (4.3)$$

At order  $E^{1/2}$ , we recover (3.11), (3.21) and (3.22), and at order  $E$  we find

$$U_z = \frac{dz}{dp}. \quad (4.2)$$

where the geostrophic velocity,  $U(z)$  is the horizontal average of  $u$ , so that  $\underline{u} = 0$ . On substituting (4.1) into (2.31) - (2.35) and equating like powers of  $E$ , we find that the dominant balance involves only the geostrophic flow:

$$\begin{aligned} u &= U + E^{1/2} u', & B &= I_z + E^{1/2} B', \\ T &= -z + E^{1/2} T', & p &= p + E^{1/2} p', \end{aligned} \quad (4.1)$$

Rather than attempting to eliminate the unbalanced force,  $E$ , defined in (3.20), we shall, for the remainder of this paper, include an equal but opposite viscous force set up by the geostrophic shear,  $U$ . This dynamical balance can be demonstrated by scaling solutions of (2.31) - (2.35) in the following way:

Figure 1. Taylor's constraint automatically, so the criteria (3.40) and (3.51) are not relevant for these modes. The dashed curve labelled  $r_T$  in Figure 1 gives the Taylor states with wavenumbers corresponding to the dashed extension of the  $l \neq 0$  linear curve below  $A = 4$ . These wavenumbers are given by (3.17) with  $\frac{1}{2} \leq X \leq \frac{3}{2}$ . In this range, the linear  $l \neq 0$  solutions are at a local minimum of the Rayleigh number, but not at a global minimum, which is given by  $l = 0$  modes. If one adopts the simple philosophy that the wavenumbers selected should be those that give the smallest Rayleigh number at onset, and that these wavenumbers should be retained as the Rayleigh number increases, these Taylor states will never occur. Nevertheless, we have included them as a dashed curve in Figure 1 because it may be that stability considerations will indicate that the wavenumbers that actually arise as  $r$  is increased move away from their values at onset. It is also interesting to note how closely the inequality (3.51) is approached by the Taylor solutions shown in Figure 1.

#### 4. BOUSSINESQ SCALINGS

$$\mathbf{U} = U(z) \mathbf{l}_z,$$

on the walls. This has the consequence that  $U_y \equiv 0$ , and in future we shall write two preferred rolls must be excited to equal amplitude as otherwise  $U_y$  would be nonzero. walls make themselves felt when  $A > 4$ : a single oblique roll is no longer a possibility. The an Ekman pumping at the walls, this pumping is insinuating, as we shall see below. The though, in the case of no-slip surfaces, the nonzero  $y$ -vorticity of the  $l = 0$  roll creates either case the preferred  $l = 0$  modes ("bananas") are still possible when  $A < 4$ . In this section and throughout §5 we shall suppose instead that they are no-slip surfaces. in this section and first consider the case in which the vertical walls are slippery, but later  $B_0$ ). We shall at first consider the case in which the  $x$ -direction (i.e. parallel to in dimensionless variables, the layer is still bounded by  $\mathbf{l}$  by vertical walls,  $y = 0$ ,  $L$  layer will be confined horizontally in the direction defined by  $\mathbf{l}$  by vertical walls,  $y = 0$ ,  $L$  We shall henceforward consider only duct models, by which we mean that the convecting main theoretical challenge.

As for the system (3.10) - (3.14), solutions exist of the form (3.15). The basic idea is that the solution will, through the nonlinearity of (4.3), equilibrate to a steady ( $w = 0$ ) state. And it is the determination of this state that provides the or a periodic ( $w \neq 0$ ) state. Since, however, the excitation of convection in the layer cannot create horizontal momentum, we can supplement the latter of which determines  $\mathbf{U}$  only to an additive constant. Since, however, the excitation of convection in the layer cannot create horizontal momentum, we can supplement (2.36f) by

which removes the arbitrary constant.

$$\text{stress-free: } \int_1^0 U dz = 0, \quad (4.10)$$

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$$\text{stress-free: } \frac{\partial U}{\partial z} = 0, \quad \text{at } z = z_0, 1 + z_0, \quad (4.9f)$$

$$\text{no-slip: } U = 0, \quad \text{at } z = z_0, 1 + z_0, \quad (4.9r)$$

Supplemental to the derivation of boundary conditions in §2, we note here that the geostrophic flow should obey

while  $(\nabla \times \mathbf{B}) \times \mathbf{B}^H$  and  $\mathbf{U}$  tend to finite limits.

subject to appropriate boundary conditions. By re-introducing the viscosity (into the determination of the geostrophic flow) we have not automatically ruled out the possibility of a Taylor state. As such a state is approached, the magnitude of  $\mathbf{B}$ , tends to infinity while  $(\nabla \times \mathbf{B}) \times \mathbf{B}^H$  and  $\mathbf{U}$  tend to finite limits.

$$\nabla \cdot \mathbf{B}' = 0, \quad (4.8)$$

$$\frac{\partial T'}{\partial t} + \mathbf{U} \cdot \nabla T' = \Delta^2 T' - \tau u_z, \quad (4.7)$$

$$\frac{\partial \mathbf{B}'}{\partial t} + \mathbf{U} \cdot \nabla \mathbf{B}' = \nabla \times (\mathbf{u} \times \mathbf{l}_z) + \Delta^2 \mathbf{B}', \quad (4.6)$$

$$\mathbf{l}_y \times \mathbf{u} = -\Delta p' + T'_z + A(\nabla \times \mathbf{B}') \times \mathbf{l}_z, \quad (4.5)$$

$$\Delta \cdot \mathbf{u} = 0, \quad (4.4)$$

We have now transformed our problem into that of solving the fully nonlinear (4.3) and

$$\frac{d^2U}{dz^2} = \frac{2(k_z^2 + l^2)}{1 - \frac{d}{k_z^2}} \left\{ l^2 (u_z B^* + u_z^* B) + ik_3 A \left( B \frac{dB^*}{dz} - B^* \frac{dA}{dz} \right) \right\}. \quad (4.15)$$

In the case of slippery vertical walls, we have from (4.3)

$$\frac{d^2}{dz^2} \left( \frac{d^2U}{dz^2} - k_z^2 - l^2 \right) T = i(\omega + kT) \frac{d^2z}{dz^2} + r u_z. \quad (4.14)$$

$$\frac{d^2}{dz^2} \left( \frac{d^2z}{dz^2} - k_z^2 - l^2 \right) B = i(\omega + kT) B - r u_z, \quad (4.13)$$

$$\begin{aligned} & + Ak_z^2 \frac{dU}{dz} + Ak_z^2 \frac{dz}{dz} \left( \frac{l^2}{k_z^2 + l^2} T + \frac{A^2 k_A^2}{l^2 - u_z^2} \right. \\ & \left. \left( \frac{d^2z}{dz^2} - k_z^2 - l^2 \right) u_z = i(\omega + kT) \left[ u_z - \frac{A^2 k_A^2}{l^2 - u_z^2} B \right] \right) \end{aligned} \quad (4.12)$$

After eliminating  $u_z$ ,  $B_z$ , and  $B^*$  from (4.4) – (4.8) (and after omitting the  $'$  and the  $''$  as before), we obtain

the presumption that these walls are perfect electrical conductors.

take  $l = 1$ ,  $u_z$  and  $B_z$  vanish together on the vertical walls. Implicit in (4.11) is therefore By (4.11) and the  $u_z$  given by (3.30), we see that, if  $l$  is an odd integer (we shall always

$$B_z(x, y, z, t) = ikB_z(z) \exp[i(kx + wt)] \cos ly + c.c.. \quad (4.11)$$

$B_z$  alone, modify (3.30), writing instead

$k$  and  $l$ , and we shall therefore take  $L = \pi/1.668 \approx 1.883$ . In what follows, we shall, for convenience in an unbounded layer. We shall therefore concentrate here on these values of  $k$  and  $l$ , so that  $l$  was an integer (or zero) for all solutions considered. For this choice  $k = 1.117$  and  $l = 1.668$  define the preferred mode of marginal Boussinesq convection in an unbounded layer,  $\pi/1.668$  defines the preferred mode in this paper, however,  $A = 6$  and  $u/l$ . In Paper I, we chose  $L = \pi$ , so that  $l$  was an integer (or zero) for all solutions considered. Electrically conducting and thermally insulating, and that they are placed at  $y = 0$  and it convenient to suppose that the vertical walls of the duct are impermeable, perfectly electrically conducting and thermally insulating, and that they are placed at  $y = \pi/2$ . We therefore quantities vanish simultaneously whenever  $y$  is an integral multiple of  $\pi/2$ . We see that these quantities vanish simultaneously whenever  $y$  is an integer multiple of  $\pi/2$ . From the expressions for  $u_z$ ,  $B_z$ , and  $Q_T/\partial y$  corresponding to (3.30), we see that these to consider both the case of slippery vertical walls (§6) and no-slip vertical walls (§5). whose convective cores are confined by surrounding mantles (see §1). We therefore wish expect in the convective regimes of bodies like stars, that have free surfaces, and planets, wish to introduce vertical walls to explore in a planar model the differences that might be star or planet. The axisymmetric "dougbnut" mode,  $k = 0$  is still possible. Second, we in an equatorial belt can only take discrete values, dictated by the circumference of the limited latitudinal extent of the applications. The longitudinal wavenumber of convection spherical convective zone, and we therefore wish to impose a "cut-off" that stimulates the early applications in mind (see §1), we wish to model only the equatorial regions of a ignoring the suffix  $z$  on  $U_z$ .

$$\begin{aligned} u &= U + cE_1/4u, & B &= I_z + cE_1/4B, \\ T &= -z + cE_1/4T, & p &= p + cE_1/4p, \end{aligned} \quad (4.18)$$

The scaling replacing (4.1) is now which is the dimensional form of (4.17).

$$U = \frac{2U_{p0\mu}}{L} \left( \frac{u}{U} \right)^{1/2} [(\nabla \times B) \times B],$$

so that

The resulting mass flux  $WL$  can be balanced only by an equal but opposite mass flux in the Ekman layers on the vertical walls. Each Ekman layer carries the flux  $-(v/4U)^{1/2}U$ ,

$$W = \frac{2U_{p0\mu}}{L} [(\nabla \times B) \times B].$$

In deriving (4.17), we temporarily revert to dimensional units. When viscosity is omitted from the equation of motion, the force  $\mu^{-1}[(\nabla \times B) \times B]$  is balanced by the Coriolis force created by a vertical motion,  $W(z)I_z$ , in the bulk of the layer, given by

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$\Delta^2 U$  does not appear in (4.3) nor the  $d^2 U/dz^2$  in (4.15).

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$$U = \frac{2(k_2 + l_2)}{l} \int_z^0 \left\{ l^2 (u_z B^* + u^{*z} B) + ik_3 A \left( B \frac{dB^*}{dz} - B^* \frac{dB}{dz} \right) dz + Dz \right\}$$

no-slip at the walls, we see from (4.9f) that where the constant  $C$  is chosen so that  $dU/dz$  vanishes at the walls. If however there is

$$U = \frac{2(k_2 + l_2)}{l} \int_z^0 \left\{ l^2 (u_z B^* + u^{*z} B) + ik_3 A \left( B \frac{dB^*}{dz} - B^* \frac{dB}{dz} \right) dz + C \right\}$$

Bearing in mind (4.9f) and (4.10f), we see that in the case of stress-free walls

In Fig. 2(b),  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  are shown, where  $a_{\max} \approx 3.055$ ,  $B_{\max} \approx 0.351$  and  $\gamma_{\max} \approx 11.185$  are the maximum (central) values of  $a$ ,  $B$  and  $\gamma$ . It may be noted that  $B$  does not vanish at  $z = 0$  and 1, as we have imposed the boundary conditions (3.41) for insulating horizontal walls. The phases,  $\theta$ ,  $\phi$  and  $\psi$  of  $u_z$ ,  $B$  and  $T$  are shown in Fig. 2(c). The variation in phase is rather small in this case; this is not surprising as they would all be exactly in phase in the linear Boussinesq case.

$$u_z(z) = a(z)e^{i\theta(z)}, \quad B(z) = B(z)e^{i\phi(z)}, \quad T(z) = \gamma(z)e^{i\psi(z)}. \quad (5.1)$$

The fields  $u_z$ ,  $B$  and  $T$  are shown in Figures 2 and 3 through their amplitudes and phases: The amplitudes seem to be relevant in the case of a rigid duct, even for finite amplitude states, symmetries seem to be relevant in the case of a rigid duct, even for finite amplitude states, and the geostrophic flow,  $U$ , is antisymmetric. In fact only steady solutions with these solutions,  $|u_z|$ ,  $|B_z|$  and  $|T|$  are all symmetric about the central horizontal plane,  $z = \frac{L}{2}$ , supercritical. In the Boussinesq approximation, the frequency,  $\omega$ , is zero for all marginal Rayleigh number,  $r$ , for  $A = 6$  is 43.637, so that the case depicted in Figs. 2 is only mildly preferred over the rolls aligned with the rotation axis ( $l = 0$ ). The critical value of the choice  $A = 6$  is large enough ( $> 4$ ) to ensure that the oblique rolls ( $l \neq 0$ ) are horizontal from  $y = 0$  to  $y = \pi/l \approx 1.883$ , in units in which the layer depth is 1. To fit this solution into the duct, the duct must extend in an infinite layer when  $A = 6$ . These wavenumbers being those minimizing the Rayleigh number for marginal convection Figures 2 and 3. In both these sets of figures,  $A = 6$ ,  $k = 1.117$  and  $l = 1.668$ , The results of numerical integration (4.12) - (4.14) and (4.20) are presented in Figures 2 and 3. These wavenumbers being those minimizing the Rayleigh number for marginal convection in an infinite layer when  $A = 6$ ,  $k = 1.117$  and  $l = 1.668$ , Figures 2 and 3. In both these sets of figures,  $A = 6$ ,  $k = 1.117$  and  $l = 1.668$ , The results of numerical integration (4.12) - (4.14) and (4.20) are presented in

consider the simpler case in which (2.41) apply. on the case of electrically insulating horizontal boundaries, although we shall briefly also depend on the mechanical conditions at the horizontal boundaries. We shall focus mainly conductors and perfect thermal insulators. As already mentioned, the results will not vertical walls will be investigated here, these walls being (as always) perfect electrical adjectives "rigid" in the title of this section indicates that only the case of sticky viscous layers are required in which the flow can adjust to the no-slip or stress-free conditions at the horizontal boundaries.

## 5. THE RIGID DUCT

The mainstream geostrophic flow satisfies (4.10) but neither of the conditions (4.9); thin viscous layers are required in which the flow can adjust to the no-slip or stress-free conditions at the horizontal boundaries.

$$U = -\frac{1}{l^2} \frac{d}{dz} \left\{ l^2 (u_z B^* + u_z^* B) + ik^3 A \left( B \frac{dB^*}{dz} - B^* \frac{dB}{dz} \right) \right\}. \quad (4.19)$$

The vector equations (4.4) - (4.8) and their scalar consequences (4.12) - (4.14) follow as before, but (4.15) is replace by the scaled form of (4.17), i.e.

$$\epsilon = \left( \frac{T}{d^{1/2}} \right)^{1/2}$$

where  $\frac{L}{d}$  is the aspect ratio of the duct:

$$U = - \frac{2}{1} \frac{dz}{d} (u_z B_* + u_* B). \quad (5.6)$$

$$\frac{d^2 T}{dz^2} = \frac{\delta}{i(U - \omega) L} - W, \quad (5.5)$$

$$\frac{d^2 B}{dz^2} = i(U - \omega) B - u_z, \quad (5.4)$$

$$\frac{d^2 u_z}{dz^2} = i(U - \omega) u_z - T, \quad (5.3)$$

When (4.12) – (4.14) and (4.20) are scaled as in (5.1) and the limit  $r \rightarrow \infty$  is taken and the  $\tau$  is omitted, it is found that

so that the solutions correspond to convection with a large number of rolls in the vertical direction. Fig. 3(c) are almost identical for all three variables; there is a large variation in phase, same figure, without dividing by their maxima for normalization. The phase plots shown of our asymptotic scaling (5.2), all these amplitudes can be conveniently plotted on the same figure, with the amplitudes of  $u_z$ ,  $B$  and  $T$  displayed in Fig. 3(b). Note that, because present in the amplitudes of  $u_z$ ,  $B$  and  $T$  displayed in Fig. 3(b). Similar oscillations are present near the boundaries [see Fig. 3(a)]; in the central regions there are relatively weak oscillations, whose amplitude decreases towards the centre of the layer. In the asymptotic limit, and is largest near the boundaries [see Fig. 3(a)].

The geostrophic wind remains antidiabatic about  $z = \frac{1}{2}$  in the asymptotic limit, and

bers as for Figs. 2, we have  $z_1 = 50$ .

With the stated choice of  $r$ , and adopting the same values of Elsasser number and wavenum-

$$z_1 = \frac{k_{1/2} (k_2 + l_2)^{1/2}}{A_{1/4} r^{1/4}}.$$

In this scaling the horizontal boundaries are  $z = 0$  and  $z_1$ , where

$$\begin{aligned} U &\leftarrow \frac{l}{(k_2 + l_2)^{1/2}} \frac{1}{A_{1/2} r^{1/2}}, \\ T &\leftarrow -T \frac{(k_2 + l_2)^{3/8}}{k_{3/4}^{13/4} A_{-1/8} r^{7/8}}, \\ B &\leftarrow B \frac{(k_2 + l_2)^{3/8}}{k_{3/4}^{13/4} A_{-1/8} r^{-1/8}}, \\ u_z &\leftarrow u_z \frac{l^{7/4}}{k_{1/4} (k_2 + l_2)^{7/8}} \frac{1}{A_{3/8} r^{3/8}}, \\ z &\leftarrow z \frac{k_{1/2} (k_2 + l_2)^{1/4}}{l^{1/2}} \frac{1}{A_{-1/4} r^{-1/4}}, \end{aligned} \quad (5.2)$$

Figure 3 is for a case of very large  $r$ , namely  $r = 576,503$ . As  $r$  is increased, an asymptotic limit is approached, and a number of terms in the full equations (4.12) – (4.14) become unimportant (see below). It is then possible to solve the equations using the scaling

Since  $\beta(z) = \beta(z_1 - z)$ ,  $\beta$  decreases symmetrically to zero as  $z$  increases from  $\frac{1}{2}z_1$  to  $z_1$ . When  $\beta$  differs only slightly from  $\sqrt{2}$ ,  $\beta$  is approximately constant (and equal to  $\beta_0$ ) in a mainstream away from the walls, and matches to conditions (5.13) in thermal boundary

$$\text{z}_1 = \frac{4\sqrt{3}}{\beta_0} \int_1^0 \frac{\sqrt{(1-u_2)(V-u_2-u_4)}}{du}. \quad (5.15)$$

According to (5.14),  $\beta$  increases monotonically with  $z$  up to a maximum of  $\beta_0$  ( $\leq \sqrt{2}$ ) at  $z = \frac{1}{2}z_1$ , where

$$V = \frac{\beta_0}{12} - 1.$$

where

$$z = \frac{2\sqrt{3}}{2\beta/\beta_0} \int_{\beta/\beta_0}^0 \frac{\sqrt{(1-u_2)(V-u_2-u_4)}}{du}, \quad (5.14)$$

The relevant solution of (5.12) and (5.13) is

$$\beta = 0, \quad \text{at } z = 0, z_1. \quad (5.13)$$

which must be solved subject to

$$\frac{d^2\beta}{dz^2} = \frac{4}{1}\beta_0 - \beta, \quad (5.12)$$

and

$$\frac{d\beta}{\phi} = -\frac{2}{1}\beta^2, \quad (5.11)$$

substitute into (5.8) and (5.9), and equate real and imaginary parts. We obtain

$$B(z) = \beta(z)e^{i\phi(z)}, \quad (5.10)$$

Let us again adopt the polar representation (3.26):

$$B = 0, \quad \text{at } z = 0, z_1. \quad (5.9)$$

which must be solved subject to the two conditions

$$\frac{d^2B}{dz^2} = -i\frac{dz}{p}(BB^*)B - B, \quad (5.8)$$

equation, for all  $z$ , we reduce both equations and boundary conditions to the single second order

$$u_z = B = T \quad (5.7)$$

then by assuming that  $g = 1$  (the only case considered here) and the illustrative conditions (4.22) apply. For Equations (5.3) - (5.6) for the asymptotic state are solved with particular ease when  $w = 0$  in (5.3) - (5.5).

It follows from (5.23) that to leading order the right-hand side of (5.24) can be neglected, so that  $\xi \approx A_0 + A_1 z$ . Since however the solution should remain near  $\xi = 0$ , it follows that the constant  $A_1$  is zero.

$$\frac{d^2\xi}{dz^2} = -\frac{2}{i}\frac{d}{d\xi}(u_z B^* + u^*_z B). \quad (5.24)$$

and by (5.18) and (5.19), we have

$$\frac{d^2}{dz^2}(u_z B^* + u^*_z B) = O(\xi), \quad (5.23)$$

but will become  $O(1)$  as either boundary is approached. By (5.21), between  $u_z$  and  $B$  in the expectation that  $\xi$  will be vanishingly small in the limit  $r \rightarrow \infty$

$$\xi = u_z - B, \quad (5.22)$$

oscillations we introduce the difference,  $\xi$  is very large, and one might expect the leading to dominate completely. To study these, these leading order parts. This is slightly surprising, as the Rayleigh number used for Fig 3 has significant oscillations superimposed on the numerical solutions shown in Fig 3 have significant oscillations superimposed on

$$u_z \sim B \sim B_0 e^{-iz}, \quad (5.21)$$

To leading order, (5.7) remains true outside the boundary layers, and

$$u_z = \frac{\partial B}{\partial z} \mp \sqrt{(k^2 + l^2)} B = 0, \quad \text{at } z = \frac{1}{2} \mp \frac{i}{2}. \quad (5.20)$$

subject to

$$\frac{d^2B}{dz^2} = -\frac{2}{i}\frac{d}{d\xi}(u_z B^* + u^*_z B) - u_z, \quad (5.19)$$

$$\frac{d^2u_z}{dz^2} = -\frac{2}{i}\frac{d}{d\xi}(u_z B^* + u^*_z B) - u_z, \quad (5.18)$$

is still admissible. We are then faced with solving (5.3) and (5.4), i.e.

$$T = u_z, \quad (5.17)$$

When solving (5.3) – (5.5) subject to the more realistic conditions (3.41), corresponding to electrically insulating walls, it is at once clear from (3.41) that (5.7) is untrue, but

$$e^{-2z} = \sqrt{2} - \beta \left[ \sqrt{[3(\beta^2 + 4)] + 2\sqrt{2}} - \beta \right]. \quad (5.16)$$

layer solution is easily obtained by setting  $\beta_0 = \sqrt{2}$  in (5.14), so obtaining layers whose thicknesses, in the original  $z$  variable, are  $O(r^{-1/4})$ ; see (5.1). The boundary

We recall here that we are interested in providing an explanation of the deviation in  $B$  from  $u_z$  as  $z$  increases from the boundary layer at  $z = 0$ , this increase being accompanied by a decrease in  $A_0$ .

$$\left( \frac{dA_0}{dz} \right)_2 = \left( \frac{8\beta_0^2 - 6}{3\beta_0} \right)^2 A_0 + k_3. \quad (5.30)$$

The relevant solution to (5.29) is real, and an integration of (5.29) gives

$$\frac{d^2 A_0}{dz^2} = 2 \left( \frac{8\beta_0^2 - 6}{3\beta_0} \right)^2 |A_0|^2 A_0. \quad (5.29)$$

We are now in a position to work to order  $\epsilon^3$ , and, by picking out the secularity of that order in (5.24), to find the slow variation of  $A_0$ . We obtain

$$f = - \frac{8\beta_0^2 - 6}{3\beta_0 \epsilon^2} A_0 [A_0 e^{iz} - A_0^* e^{-iz}].$$

Substituting these and (5.25) into (5.24), working to order  $\epsilon^2$ , and integrating once, we obtain

$$B = \beta_0 e^{-iz} + \frac{e(6 - 5\beta_0^2)}{8\beta_0^2 - 6} A_0 + \frac{e\beta_0^2}{8\beta_0^2 - 6} A_0^* e^{-2iz},$$

$$u_z = \beta_0 e^{-iz} + \frac{3e\beta_0^2}{8\beta_0^2 - 6} A_0 + \frac{e\beta_0^2}{8\beta_0^2 - 6} A_0^* e^{-2iz},$$

$$(5.28)$$

and after evaluating the constants  $k_1$  and  $k_2$  we find that (5.26) is in fact

$$w = k_1 + k_2 e^{-2iz},$$

This admits a solution of the form

$$\frac{d^2 w}{dz^2} + w = \beta_0^2 \left\{ \left[ w - \frac{1}{2} e A_0 - i \frac{dw}{dz} \right] - e^{-2iz} \left[ w^* - \frac{1}{2} e A_0^* + i \frac{dw^*}{dz} \right] \right\}. \quad (5.27)$$

where  $w = O(\epsilon)$ . On substituting (5.26) into (5.18) and (5.19), and retaining terms of order  $\epsilon$ , we find

$$B = \beta_0 e^{-iz} + w - e A_0,$$

$$u_z = \beta_0 e^{-iz} + w,$$

$$(5.26)$$

where  $e$  is a measure of the amplitude of  $\xi$  and  $\zeta = ez$  is a stretched coordinate. Now

$$\xi = e A_0(\xi) + e^2 f + e^3 g + \dots, \quad (5.25)$$

In the next approximation,  $A_0$  is a slowly varying function of  $z$ , and we therefore write

the original time-independent branch turns round at a saddle-node bifurcation  $B_4$ , and as waves with equal and opposite phase velocities. After undergoing the bifurcation  $B_3$ , to convection that mainly takes place in the lower half of the layer. Both solutions travel convection that occurs primarily in the upper half of the layer, while the other corresponds to where  $1$  and  $2$  refer to the different solutions. Typically, one solution corresponds to which are asymmetric in the sense that  $f(z) \neq -f^*(1-z)$ , although  $f_1(z) = -f_2^*(1-z)$  symmetry-breaking bifurcation,  $B_1$ , at  $r = 304.378$  two time-dependent solutions emerge from the bifurcation point,  $B_1$ , at  $r = 43.637$  is steady and symmetric. But, from the in Fig. 4, in which  $A = 6$ ,  $k = 1.117$  and  $l = 1.668$  as before, the solution emerging in the case of a rigid duct, all solutions were steady and  $f = u_z$ ,  $B$  and  $T$  all satisfied  $f(z) = -f^*(1-z)$ , while the geostrophic wind was antisymmetric:  $U(z) = -U(1-z)$ . In the case of a free duct and the occurrence of a symmetry-breaking bifurcation in the case of a free duct (§5), namely the occurrence of a symmetry-breaking bifurcation in the case of a rigid duct,  $U$  is chosen so that the mean value of  $U$  is zero) are presented in Figures 4 - 7. Fig. 4 displays an essential difference between the free duct and the rigid duct. In the case of a free duct, all solutions were steady and  $f = u_z$ ,  $B$  and  $T$  all satisfied  $f(z) = -f^*(1-z)$ , which  $A = 6$ ,  $k = 1.117$  and  $l = 1.668$  as before, the solution emerging from the bifurcation point,  $B_1$ , at  $r = 43.637$  is steady and symmetric. But, from the

$$U = \frac{2(k_2 + l_2)}{l} \int_z^0 \left\{ l^2 (u_z B^* + u_z^* B) + ik^3 A \left( B \frac{dz}{dB^*} - B^* \frac{dz}{dB} \right) \right\} dz + C, \quad (6.1)$$

The results of numerical integrations of (4.12) - (4.14) and (4.16f), i.e.

the case of electrically insulating horizontal boundaries. We shall consider only depend on the mechanical conditions at the horizontal boundaries. The results will not conductors and perfect thermal insulators. As already mentioned, the results will not vertical walls will be investigated here, these walls being (as always) perfect electrical conductors and perfectly insulated. For large  $r$ , the forms (5.32) then agree with the numerical results over a wide range of  $z$ . This analysis indicates why the oscillations persist at such large values of  $r$ : the oscillatory terms decay at only the slow rate  $1/z$  as  $z \rightarrow \infty$ , and  $z$  itself is scaled only on  $r^{1/4}$ .

This theory is unable to decide on the value of the constant  $\zeta_0/e$ , but numerical integrations can be used to determine it approximately. For large  $r$ , the forms (5.32) then agree with the numerical results over a wide range of  $z$ . This analysis indicates why the oscillations persist at such large values of  $r$ : the oscillatory terms decay at only the slow rate  $1/z$  as  $z \rightarrow \infty$ , and  $z$  itself is scaled only on  $r^{1/4}$ .

$$B = B_0 e^{-iz} + \frac{3B_0(z - \zeta_0/e)}{1} (6 - 5B_0^2 + B_0^2 e^{-2iz}), \quad (5.32)$$

$$u_z = B_0 e^{-iz} + \frac{3(z - \zeta_0/e)}{B_0} (3 + e^{-2iz}),$$

where  $\zeta_0$  is an  $O(1)$  constant. Substituting this result into (5.28) we find that

$$A_0 = \frac{3B_0(\zeta_0 + ez)}{8B_0^2 - 6}, \quad (5.31)$$

$\zeta_0 = 0$  in (5.30) and integrate once more to obtain by a decrease in  $|G|$ . We therefore seek a non-oscillatory solution of (5.30), and so take

amplitude peaks are shifted nearer to  $z = 1$  where the geostrophic wind is strongest. Geostrophic velocity  $U$  that is larger in absolute value near  $z = 1$  than near  $z = 0$ . The other branch,  $w = -4.932$  (it therefore propagates in the positive  $x$ -direction), and has a case shown) than at the other. The value of  $w$  in our dimensionless units is 4.932, so that the wave propagates in the negative  $x$ -direction. For the corresponding solution from the case shown) is no longer antisymmetric, but is larger in amplitude at one boundary ( $z = 0$  in the case shown) than at the other. The value of  $w$  in our dimensionless units is 4.932, so that these figures are scaled in the same manner as were Figs. 2 and 5. The geostrophic wind shows the solution shortly after it has undergone the symmetry-breaking bifurcation at  $B_3$ . These figures are plotted in the form of the geostrophic wind, the mildly supercritical cases  $r = 50$  for rigid and free ducts are very similar. Figure 6 is for  $r = 320$ , and apart from a slight change in the form of the geostrophic wind, the mildly supercritical cases  $r = 50$  for rigid and free ducts are very similar. Figure 6 is for  $r = 320$ , and in Figs. 5, solutions are plotted in a manner complete analogy analogous to that used in Figs. 2.

In Figs. 5, solutions are plotted near the bifurcation points  $B_1$  and  $B_2$ . They show the correct  $(r - r_c)^{1/2}$  behaviour near the bifurcation points  $B_1$  and  $B_2$ .

Although in principle any measure of the amplitude suffices, in practice some care must be exercised. If a does not contain any contribution from  $a_3$  and  $a_4$ , the two branches must be exchanged from  $B_3$  will coincide in the  $(r, \alpha)$ -plane; if the symmetric part of  $a$  does not contain a contribution from both  $a_1$  and  $a_4$ , the bifurcation diagram will not necessarily be exchangeable. If  $a$  contains any contribution from  $a_3$  and  $a_4$ , the two branches must be exchanged. In Figs. 5, solutions are plotted near the bifurcation points  $B_1$  and  $B_2$ .

$$a = a_1 - a_2 + a_3 - a_4.$$

The amplitude used in Fig. 4 is defined by

$$a_1 \sim a_1, \quad a_2 \sim -a_2, \quad a_3 \sim -a_3, \quad a_4 \sim a_4.$$

so that by (6.2)

$$\omega \sim -\omega, \quad u_{r^*}^z \sim u_{r^*}^z, \quad u_{r^*}^z \sim -u_{r^*}^z, \quad u_{i^*}^z \sim -u_{i^*}^z, \quad u_{i^*}^z \sim u_{i^*}^z,$$

For steady solutions  $a_2 = a_3 = 0$ . All four are in general nonzero for time-dependent solutions; the two solutions for the same Rayleigh number are related by

$$a_1 = \int_{1/2}^0 u_{r^*}^z dz, \quad a_2 = \int_{1/2}^0 u_{r^*}^z dz, \quad a_3 = \int_{1/2}^0 u_{i^*}^z dz, \quad a_4 = \int_{1/2}^0 u_{i^*}^z dz. \quad (6.2)$$

Steady solutions ( $\omega = 0$ ) have the property that, with the correct choice of phase,  $u_{r^*}^z = u_{i^*}^z = 0$ . Near the bifurcation point  $B_2$  (a two cell solution),  $u_{r^*}^z$  is zero. We define near the bifurcation point  $B_1$  (a one cell solution),  $u_{r^*}^z$  is zero, while  $u_{i^*}^z$  is zero, while

$$u^z = u_{r^*}^z + u_{i^*}^z + i(u_{i^*}^z + u_{r^*}^z).$$

The amplitude shown in Fig. 4 is based on the vertical velocity, and is constructed in the following way. We decompose  $u^z$  into its real and imaginary parts,  $u_r^z$  and  $u_i^z$ , and further divide  $u_r^z$  and  $u_i^z$  into parts that are symmetric and antisymmetric about  $z = \frac{1}{2}$ , so that

by (3.16) with  $\pi^2$  replaced by  $4\pi^2$ . Here  $B_2$  corresponds to a linear solution with two rolls in the vertical direction and a critical Rayleigh number given by (3.16) when  $\omega$  is zero at  $B_2$ . Here  $B_2$  corresponds to a continuation down to connect with the zero solution at  $B_2$ .

We now return to the subject which formed the starting point of this investigation, the extension of the linear theory of compressible rotating magnetoconvection developed in

## 7. THE FREE COMPRESSIBLE DUCT

We conjecture that these solutions are unlikely to be stable; disturbances that have a large amplitude in the mainstream and which travel with the mainstream geostrophic velocity will probably be unstable at such large Rayleigh numbers.

near the bottom boundary,  $z = 1$ .

motion in the positive  $x$ -direction, and in which convection occurs only in a boundary layer analogous solution to that shown in Figs. 7, in which  $w$  is negative, corresponding to wave too rapidly through the fluid for significant convection to occur. There is, of course, an and this is why the amplitude of the convection is so small there; the wave is moving  $w_D \equiv w + kU$  vanishes, lies within the boundary layer. In the mainstream,  $w_D$  is large, in these units, which means that the critical level, at which the Doppler-shifted frequency entirely confined to a boundary layer of thickness  $O(r^{-1/4})$ . The frequency is  $\omega = 1.0433$  The nature of the solutions shown in Figs. 7 is remarkable: the convection is almost

lines of that presented in §5. We shall not attempt to develop here an asymptotic,  $r \rightarrow \infty$ , theory along the of (6.1). These scalings reduce (4.12) - (4.14); only (5.6) is replaced by the scaled form (5.3) - (5.5) are recovered from (4.12) - (4.14), where the limit  $r \rightarrow \infty$  is taken and the  $\tau$  is omitted, advantage of scaling (6.2) is that, when the  $\tau$  is taken and the  $\tau$  is before. The horizontal boundaries scales as in §5, i.e. they are at  $z = 0$  and  $z_1$  as before. The Only the  $z$  scaling is the same as in (5.1), and this means that the position of the

$$U = \frac{1}{2} \int_z^0 (u_z B^* + u^* B) dz + C. \quad (6.4)$$

These scalings reduce (4.12) - (4.14) again to (5.3) - (5.5), where now  $w$  is nonzero after the symmetry is broken, together with

$$\begin{aligned} U &\leftarrow \tilde{U} \frac{(k^2 + t^2)^{1/2}}{A^{1/2} r^{1/2}}, \\ T &\leftarrow -\tilde{T} \frac{(k^2 + t^2)^{5/8}}{A^{1/8} r^{9/8}}, \\ B &\leftarrow \tilde{B} \frac{(k^2 + t^2)^{5/8}}{A^{1/8} r^{1/8}}, \\ u_z &\leftarrow \tilde{u}_z \frac{k^3/4 (k^2 + t^2)^{9/8}}{A^{5/8} r^{5/8}}, \\ z &\leftarrow \tilde{z} \frac{k^{1/2} (k^2 + t^2)^{1/4}}{A^{-1/4} r^{-1/4}}, \end{aligned} \quad (6.3)$$

Figure 7 presents the solutions for  $r = 576, 503$ , again scaled in the way suggested by the asymptotic theory, in which it is convenient to replace (5.2) by

Even though compressible convection occurs as waves, it was found in paper I that the eigenfunctions are not totally dissimilar from those of the Boussinesq model. We therefore

assume the vertical walls are stress-free.

The equation for the geostrophic wind is the same as in the Boussinesq case: (4.15) since

$$\left( \frac{d^2}{dz^2} - k_z^2 - l_z^2 \right) T = i(\omega + kU) \frac{\partial}{\partial z} u + ru. \quad (7.3)$$

$$\left( \frac{d^2}{dz^2} - k_z^2 - l_z^2 \right) B = i(\omega + kU) B - \frac{\partial}{\partial z}, \quad (7.2)$$

$$+ Ak_z^2 \frac{d}{dz} B + \frac{Ak_z^2 (k_z^2 + l_z^2)}{l_z^2 T}, \quad (7.1)$$

$$- \frac{(z_0 + \frac{1}{2}) \zeta_{m+1}}{ikuA} \left[ m + \frac{(m+1)(k_z^2 + l_z^2)}{l_z^2} \right] \\ \left( \frac{d^2}{dz^2} - k_z^2 - l_z^2 \right) w = i(\omega + kU) \left[ w - \frac{l_z^2 \zeta_m}{l_z^2 \zeta_{m+1}} B \right] + \frac{A^2 k_z^4}{l_z^2} w$$

$B_z$  and  $T$ . The equations satisfied by these are (2.23) to (2.28) above. As in paper I, a convenient set of dependent variables is  $w = pu_z$ , the vector form of the equations in the compressible case has been given in equations

that propagate in the negative  $x$ -direction are principally concentrated.

waves moving in the negative  $x$ -direction are principally concentrated with structure from the tenuous upper part of the layer, in which the convection associated with mainly in the lower part of the layer. When the layer is polytropic, this has a very different waves propagating in the positive  $x$ -direction are associated with convection that occurs that propagate in the positive and negative  $x$ -directions is lost from the outer. In fact, not as steady convection. In consequence, the Boussinesq symmetry between the waves Boussinesq problems is that compressible convection always occurs as a travelling wave, An important distinction, reported in paper I, between the linear compressible and linear

that minimized  $r$  in the compressible case.

preferable to introducing the slight changes that would occur had we selected the  $k$  and  $l$  on the same values of  $A$ ,  $k$  and  $l$  as we used in studying the Boussinesq limit. This seemed wave numbers  $k$  and  $l$  are both nonzero, we have, in the work described below, concentrated interest in situations where the field strongly affects the dynamics, and since then the convection zone) which was markedly affected by compressibility. Since we are primarily convection to this was the  $l \rightarrow 0$  limit (corresponding to pure banana cells in the solar even when the density varied over many scale heights within the layer. The only important minimum Rayleigh number were only slightly altered by the introduction of compressibility, The linear theory of paper I showed that the critical wave numbers determining the

of momentum, a concept that lacks some precision (see, for example, Rüdiger, 1989). The convection zone, viscous shear is normally modelled by a turbulent eddy transport is balanced by the viscous shear associated with the geostrophic flow. In application to the free duct, in which the horizontally averaged Lorentz force in the direction of the field is inappropriate to analyse the case of rigid boundaries, and we shall consider here only paper I into the nonlinear regime. Because we have in mind astrophysical applications, it

$$(7.4) \quad \int_1^0 \rho U dz = 0,$$

In Figures 9 and 10 compressible eigenfunctions are plotted in the same format as for Figure 3. Figure 9 is for the primary branch in the strongly compressible case, with  $r = 700$ , and this can be compared with Figure 10 which is for the secondary branch but at the same parameter values as Figure 9. In constructing these figures, it should be noted that the zero linear momentum condition takes the form

to  $B_3$  and  $B_4$ , which are labelled  $b_3$  and  $b_4$ . The secondary branch now bifurcates off from  $B_3$  and  $B_4$ , which are labelled  $b_3$  and  $b_4$ . The loop where the secondary branch has disappeared, still two saddle-node bifurcations corresponding to bifurcations collapsing to  $B_5$  and  $B_6$  exists. As  $z_0$  is reduced from 1 to 0, 1 these two do bifurcations correspond to  $B_5$  and  $B_6$  respectively. This is significant than for the Bousinesq case that the critical Rayleigh number for  $b_1$  is significantly greater than for the Bousinesq case,  $b_1$ , is not greater than for  $b_1$ , is not greatly changed. The only new feature is that the bifurcation from the zero solution at  $b_1$ , is now bifurcating from the primary branch, now bifurcating from the critical Rayleigh number at  $b_1$ , is not greatly changed. The move to the primary branch, we now move to the strongly compressible case,  $z_0 = 0.1$ , we see that the primary branch, in the upper half of the layer increases in strength, while that in the lower half decreases. It is now move along the secondary branch past  $B_3$  and  $B_4$ , the roll similar size and strength. As we move along the secondary branch past  $B_3$  and  $B_4$ , the pattern of the eigenfunctions. At  $B_2$ , the mode has two horizontal layers of rolls of roughly The origin of these is not so clear, but they seem to be associated with the change in the There are also two further saddle-node bifurcations on this secondary branch,  $B_3$  and  $B_6$ . and  $B_6$ .

There are also two further saddle-node bifurcations on this secondary branch,  $B_3$  and  $B_6$ . very tiny. Two saddle-node bifurcations are associated with this phenomenon, labelled  $B_5$  and  $B_6$ . At  $z_0 = 1.0$ , this loop is just visible in Fig. 8, although it is on the secondary branch. On the other hand does the symmetric branch. Consequently there has to be a loop Rayleigh number than does the asymmetric branch has, at the same amplitude, a larger situation is reversed, because the asymmetric solution, as we move further from  $B_3$ , the Rayleigh number than does the symmetric solution. As we move further from  $B_3$ , the in the Bousinesq case, the asymmetric branch has, just below  $B_3$  in Fig. 4, a smaller secondary branch first "pinches off" near  $B_3$ , and then "loops" near  $B_3$ . This is because, of the secondary mode is more complicated. As compressibility is gradually imposed, the which that one roll concentrates towards the lower, denser part of the layer. The behaviour horizontal layers of rolls, one lying above the other) evolves smoothly into a solution in vertical extent of the layer (as distinct from the solution at  $B_2$ , in which there are two branch behaves much as expected: the solution consisting of one series of rolls filling the We see in Fig. 8 that when  $z_0 = 1.0$ , the case closest to Bousinesq, the primary can be understood in general terms.

how complicated the situation can become as  $z_0$  is decreased, the behaviour of the solutions amplitude is the same as in Fig. 6, but with  $u$  replacing  $u_z$ . Although this diagram shows case ( $z_0 = 1.0$ ), and a strongly compressible case ( $z_0 = 0.1$ ). The definition of the diagram is shown for three cases: the Bousinesq case ( $z_0 \rightarrow \infty$ ), a slightly compressible ( $B_2$  on Fig. 4), while the other branch will emerge from the lowest critical Rayleigh number ( $B_1$  on Fig. 4), and that one of the branches emerging from that pitchfork bifurcation will be unfolded, and that one of the branches emerging from that pitchfork bifurcation will be expect that the symmetry-breaking bifurcation of the Bousinesq model (see Fig. 4) will

As  $r \rightarrow r_T$  the amplitude of convection rises sharply and new nonlinearities become important: in the present problem the advection of temperature and magnetic field described by  $\Delta T$  and  $\Delta B$  will dominate. For  $r < r_T$  only the geostrophic velocity  $U$ , which is purely azimuthal, makes a significant contribution to these advection processes: when  $r > r_T$ , however, the convective velocities become sufficiently large to affect the advection of convection. Advection of temperature is of course the dominant nonlinear mechanism by which the amplitude is controlled in moderate or high Froude number Rayleigh-Benard convection: in this sense, then, when  $r > r_T$  rapidly rotating magnetoconvection has a nonlinear limitting mechanism similar to that of "ordinary" convection, although the fluid motion is limited by the rotation and the magnetic field. By "ordinary" motion is meant the amplitude is controlled by the rotation and the magnetic field.

We first review the case where a Taylor state occurs at some value,  $r_T$ , of  $r$  as, for example, in the Roberts-Stewartson problem: we assume the Ekman number is small. At values of  $r < r_T$ , the amplitude of the convection is controlled by the geostrophic wind and is held to a value proportional to a positive power of the Ekman number. The precise value of this power depends on the boundary conditions.

We now turn to a value of  $r$  between the Taylor state emerges or not. The behaviour is strongly dependent on whether a Taylor state emerges or not. In §3, which apparently have no analogue in the Roberts-Stewartson problem, the nonlinearities differences appear. These are connected with the "anti-Taylor" instabilities developed in Soward (1986) and Soward and Skinner (1989) shows that in the nonlinear regime marked these two cases is not strikingly different, but a comparison of this work with that of case considered here, when rotation and gravity are perpendicular. The linear theory of original Roberts-Stewartson problem where the rotation is parallel to gravity and the perhaps the most surprising finding of this investigation is the difference between the

## 8. DISCUSSION

Although the upper regions of the layer than in the lower part of the zone. which replaces (4.10). This has the effect of making the geostrophic wind much greater in plotted, consistent with the practice of paper I. The value of  $w$  in the primary mode case is -18.022 and in the secondary mode case is 21.669. The depth at which the wavespeed equals the fluid speed is therefore much greater in the primary branch than the secondary branch. The geostrophic wind is rather small at large depth in the secondary mode, but the wavespeed is not, so these regions are being disrupted by the shear: this accounts for the small amplitudes at the base of the zone in Figure 10b. The corresponding amplitudes are much larger in Figure 9b, because the wave speed and fluid speed are there much closer at the base of the layer. It might be expected that the geostrophic wind would be smaller is driven by  $B_z$  and  $u_z$ , not  $w$ ; although  $w$  is quite small near the top of the layer  $u_z$  is considerably larger, because of the density factor. If the horizontal momentum, rather than wind speed, were plotted, there would be more symmetry between the two modes. The phases, shown in Figures 9c and 10c, are quite similar in the two cases: however, it is interesting to note that in the primary mode particularly, a substantial phase difference develops between the vertical velocity and the temperature. This feature was noted in the linear theory of paper I.

The main application of the theory of rapidly rotating magnetoconvection has been to geodynamo theory: see, for example, Fearn, Roberts and Soward (1988). It is generally accepted that, in the outer core of the Earth, Coriolis and Lorentz forces are of comparable strength, and that the viscous terms in the interior are considerably less (small Ekman number,  $E$ ). The most significant application of Taylor states, in contrast to the cases studied by Soward concerns the non-applicability of the geodynamo problem (1986) and Soward and Skinner (1989). In the second of these papers, rotation and gravity are still parallel, but the geometry is that of a cylinder rather than that of a plane layer. The significant difference between their models and ours seems to be the angle between the rotation vector and gravity. What happens in full spherical geometry is an interesting question.

but so far unresolved question: in cases where the convection is predominantly near the equatorial zone, as for example in the Braginsky (1978) model-Z dynamo, the configuration

solutions no longer have  $\exp[i(kx + ly)]$  dependence.

In the free boundary case, scalings (4.1) and (6.3) give  $r \sim E^{-4/3}$ . For values of  $r$  exceeding  $E^{-2}$ , similar considerations apply to the advection terms in the induction equation. In the free boundary case, we expect the advection terms to become significant when  $r \sim E^{-2}$ . In consequence, the amplitude of the solution increases and the advection terms will begin to very large if  $E$  is fixed initially at a small nonzero value, and  $r$  is increased. Eventually, as  $r$  becomes very large the amplitude of the solution increases, whereas the advection terms will begin to become significant. In the rigid boundary case, the scalings (4.18) and (5.2) imply that the  $(u, \Delta u)$  term is of order  $E^{1/2}, r^{3/2}$  whereas the terms retained in (4.14) are of order  $E^{1/4}, r^{11/8}$ . In consequence, we expect the advection terms to become significant when  $r \sim E^{-2}$ . This, again, as it is in ordinary convection. The mathematical problem then becomes much more difficult, as this nonlinearity couples together different horizontal modes, so that the nonlinearity of advection starts to become important.

Thus, the nonlinear mechanism of advection of temperature will start to exceed the free boundary case, scaling (4.1) and (6.3) give  $r \sim E^{-4/3}$ . For values of  $r$  exceeding  $E^{-2}$ .

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become significant. In the rigid boundary case, the scalings (4.18) and (5.2) imply that the  $(u, \Delta u)$  term is of order  $E^{1/2}, r^{3/2}$  whereas the advection terms will begin to

surface, so that magnetic field can only impede convection. It is perhaps therefore not tubes is not known. It certainly is near the surface, but rotation is unimportant near the tubes into thin tubes. Whether the flux in the deeper convection zone is in the form of thin could have very different effects on convection if one is uniform and the other is condensed between the tubes can connect in a manner which is relatively unimpeded by the fluid, and our assumptions are no longer justified. Two fields of the same mean flux density between the tubes can connect in a manner which is relatively unimpeded by the fluid, and therefore require that the flux not be expelled into thin flux tubes. If it is, the fluid number regime.

Second we require there to be a magnetic field of a suitable strength present. If this is generated by dynamo action, it is likely that the field strength will rise to a value at linear in  $B$ , so an amplifying field will grow until the nonlinear Lorentz force makes itself felt. Also the convection itself is most efficient when the Eissner number of  $O(1)$ , since then the preferred modes have wavenumbers which fill the volume available. This second requirement is therefore quite likely to be fulfilled if a dynamo occurs in a low Rossby number regime.

Third we require that the convection zones of rapidly rotating stars, and is very small in the convection zones of rapidly rotating stars, is large near the solar photosphere, but fairly small in the deeper solar convection zone, is similar to the convective velocity  $u$  and  $l$  is similar to  $d$ , then mixing length approach,  $u$ , is similar to the correlation length. If, as is generally assumed in the turbulent velocity and  $l$  is the convective velocity,  $u \sim l$ , where  $u$  scale on which the convection is occurring. If  $u$  is a turbulent viscosity,  $u \sim u^2$ , here  $d$  is the length justified. First, we require that the Ekman number  $\nu/2Ud^2$  be small; here  $d$  is the length our assumptions about the relative strength of the terms in the governing equations may be These considerations lead us to a picture of the astrophysical circumstances under which

large-scale convection velocities to the rate at which fluid can diffuse through the field. We might expect the field in these regions (which may well lie near the base of the convection zone) to vary only on a fairly long length scale; this will then restrict the photosphere. We might expect the field in these regions to disrupt and redistribute the field as happens near convection is not sufficiently strong to disrupt the toroidal field is generated, cycle, which suggests that, at least in the regions where the toroidal field is generated, the convection pattern is more in the form of elongated cells than in the form of banana cells. A further argument is made plausible by the large-scale coherence of the solar cells. The idea that the magnetic field might be significant in controlling the pattern of convection has been given further impetus by Rybes et al (1985) that completeness of rotating magnetoconvection than to a belief that the magnetic field was irrelevant. The idea that the magnetic field might be significant in controlling the pattern of convection has been given further impetus by the suggestion that the magnetic field is generated, but this may have been due more to a desire to avoid the mathematical difficulties is uncertain. Earlier models of the dynamics of the convection zone ignored greater degrees, and its role is confined to rather narrow flux tubes. The situation at convective eddies, and it is outside these active regions; the field appears to be expelled by the vigorous convection, vital in the neighbourhood of sunspots, but it is not significant the magnetic field, but this may have been due more to a desire to avoid the mathematical difficulties is uncertain. Between the photosphere and a depth of a few thousand kilometres, the solar convection, between the layers plays an important role in the dynamics of the convection is not certain that the Lorentz force plays an important role in the dynamics of the convection is, of course, vital in the neighbourhood of sunspots, but it is not significant as it is not certain that the Lorentz force plays an important role in the dynamics of the convection Jones and Holloway 1988, and paper I). The situation here is not so clear cut, however,

of gravity, rotation and field used in this paper would appear to be more relevant.

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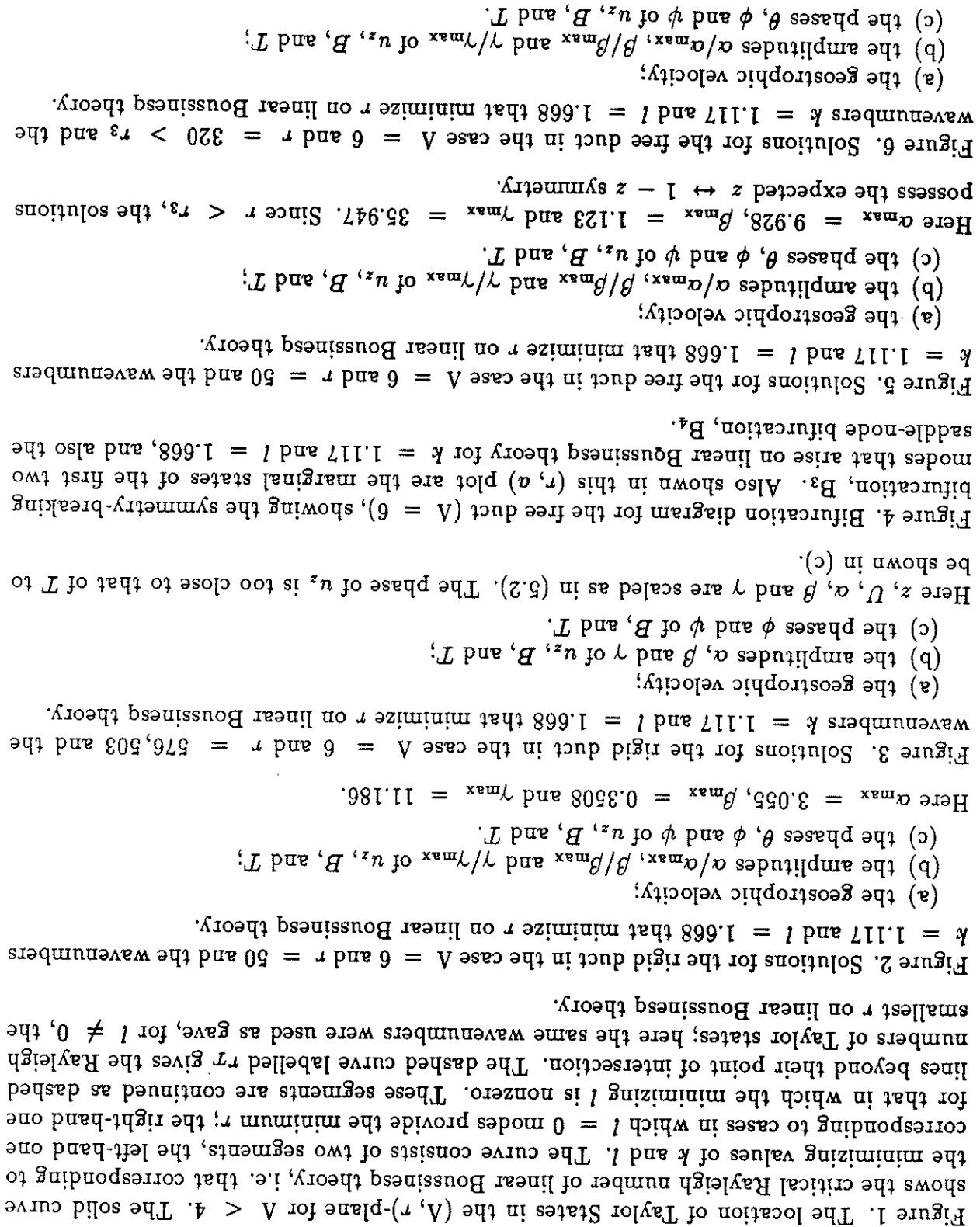
## ACKNOWLEDGMENTS

In view of their considerations we believe that our model may have some relevance to the deep solar convection zone: our plane geometry and simplified polytropic structure require us to be cautious in applying our results. Nevertheless, we should draw attention to the symmetry breaking bifurcations that occur when the rigid lid is removed (see §§6 and 7 above). In almost all previous investigations of linear and nonlinear convection with magnetic field and rotation (as in Paper I) or without them, the preferred mode of convection involved just one roll in the vertical direction. The only exceptions were models in which two or more rolls were induced in the vertical by an inhomogeneity in the equilibrium model: for example, in the two-zone model of convection were found, tropic layer was divided into a weakly superadiabatic zone at the bottom of the layer and a strongly superadiabatic zone at the top of the layer, two modes of convection were found, each dominating in one of the zones. In the nonlinear model discussed here, however, convection divides naturally into modes which exist primarily in the lower part of the zone and modes which are concentrated mainly in the upper part. This unusual behavior is a consequence of the geostrophic shear (diurnal rotation) being the controlling nonlinear effect. As the shear increases in magnitude, the convection becomes localized in the vertical. At the same time, the shear increases in magnitude (diurnal rotation) being the controlling nonlinear effect. This is an entirely compressible effect.

surprising that the convection expels the flux into tubes in order to boost its efficiency. In a rotating system at small Ekman (or Rossby) number, however, magnetic field can help release the Taylor-Proudman constraint, and hence actually promote convection (see e.g. Fearn, Rooberts and Soward, 1988). Under these circumstances it is less clear that flux expulsion will occur.

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## FIGURE CAPTIONS

Figure 10. Solutions on the secondary branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory.

Here  $a_{\max} = 673.42$ ,  $B_{\max} = 4.358$  and  $\gamma_{\max} = 1690.5$ .

- (a) the geostrophic velocity;
- (b) the amplitudes  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$ ;
- (c) the phases  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$ .

Figure 9. Solutions on the primary branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory for  $A = 6$ .

Here  $a_{\max} = 373.07$ ,  $B_{\max} = 2.911$  and  $\gamma_{\max} = 2848.0$ .

- (a) the geostrophic velocity;
- (b) the amplitudes  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$ ;
- (c) the phases  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$ .

The unfolding of the symmetry-breaking bifurcation,  $B_3$ , of (a) as  $z_0$  is decreased is evident.

Figure 8. Bifurcation diagrams for the free compressible duct in three cases:

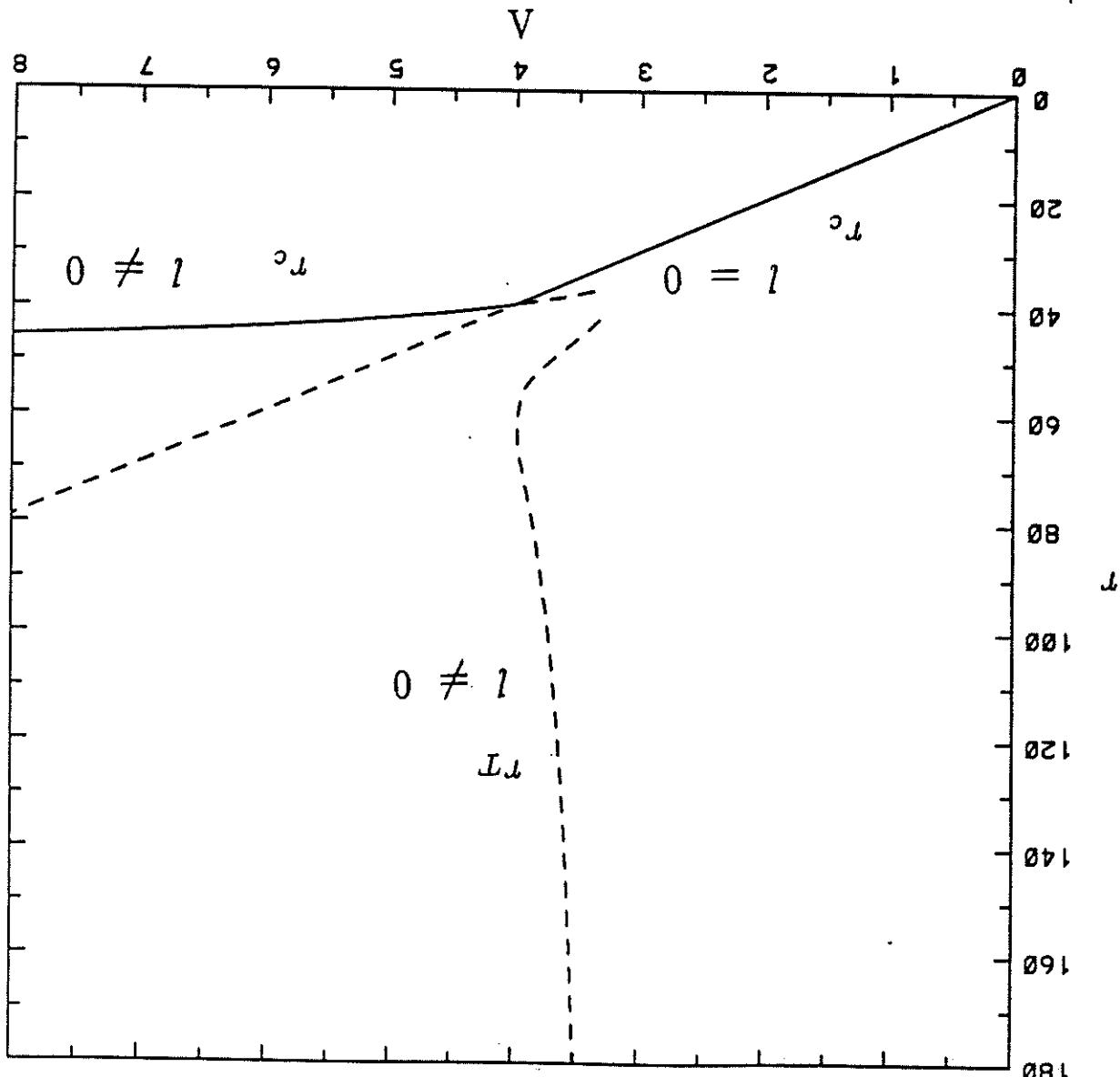
Here  $z$ ,  $U$ ,  $a$ ,  $B$  and  $\gamma$  are scaled as in (6.2).

Figure 7. Solutions for the free duct in the case  $A = 6$  and  $r = 576,503$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory.

Figure 6. Solutions for the free duct in the case  $A = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory.

Here  $a_{\max} = 153.42$ ,  $B_{\max} = 3.365$  and  $\gamma_{\max} = 1126.5$ . Since  $r > r_3$ , the solutions do not possess  $z \leftrightarrow 1 - z$  symmetry.

Figure 1. The location of Taylor States in the  $(A, r)$ -plane for  $A < 4$ . The solid curve shows the critical Rayleigh number of linear Boussinesq theory, i.e. that corresponding to the minimizing values of  $k$  and  $l$ . The curve consists of two segments, the left-hand one corresponding to cases in which  $l = 0$  modes provide the minimum  $r$ ; the right-hand one for those in which the minimizing  $l \neq 0$ . The dashed curve labelled  $r_T$  gives the Rayleigh numbers beyond their point of intersection. The dashed curve labelled  $r_T$  gives the smallest  $r$  on linear Boussinesq theory.



theory.

Figure 2(a). The geostrophic velocity for the rigid duct in the case  $A = 6$  and  $r = 50$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq

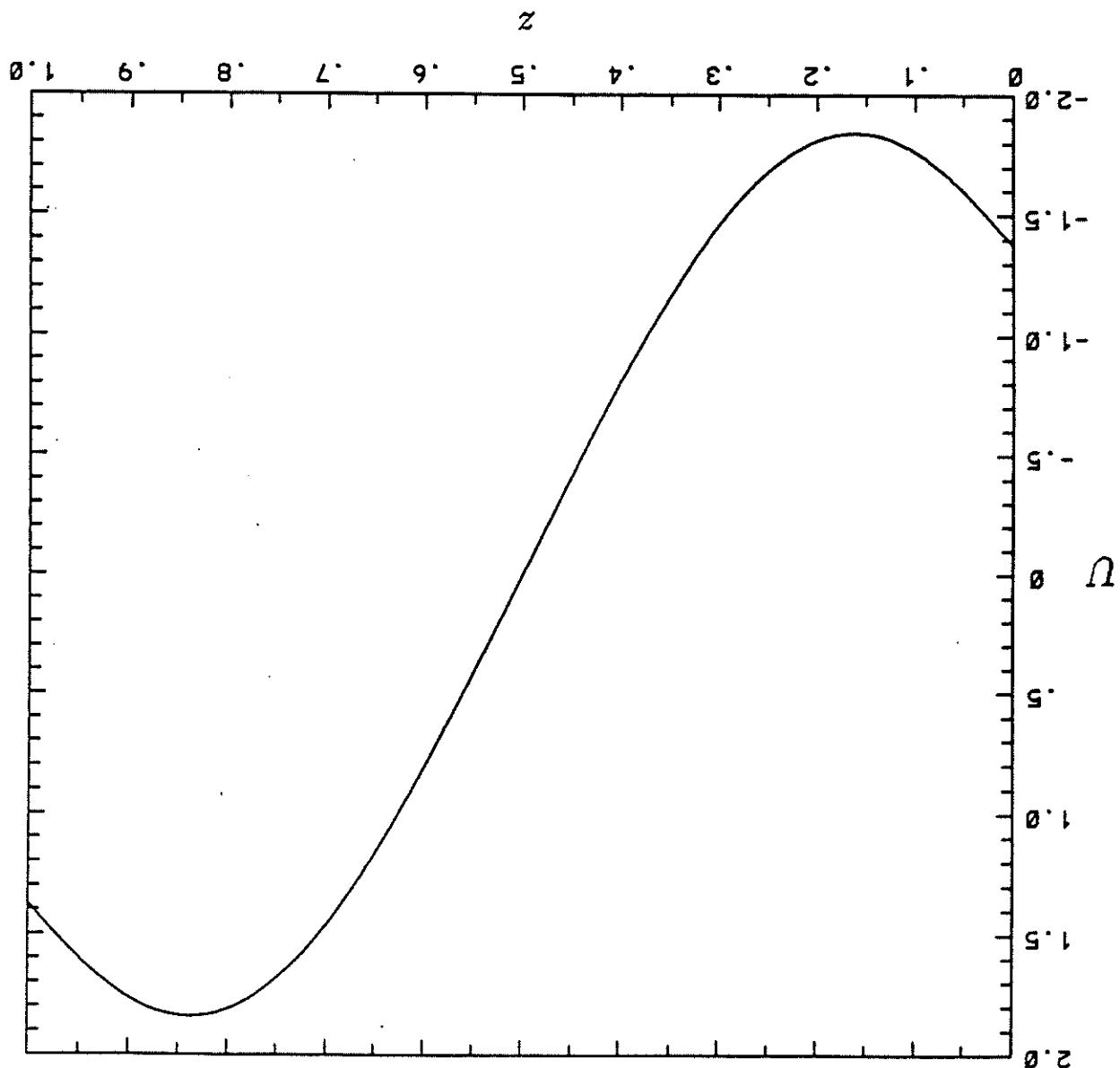
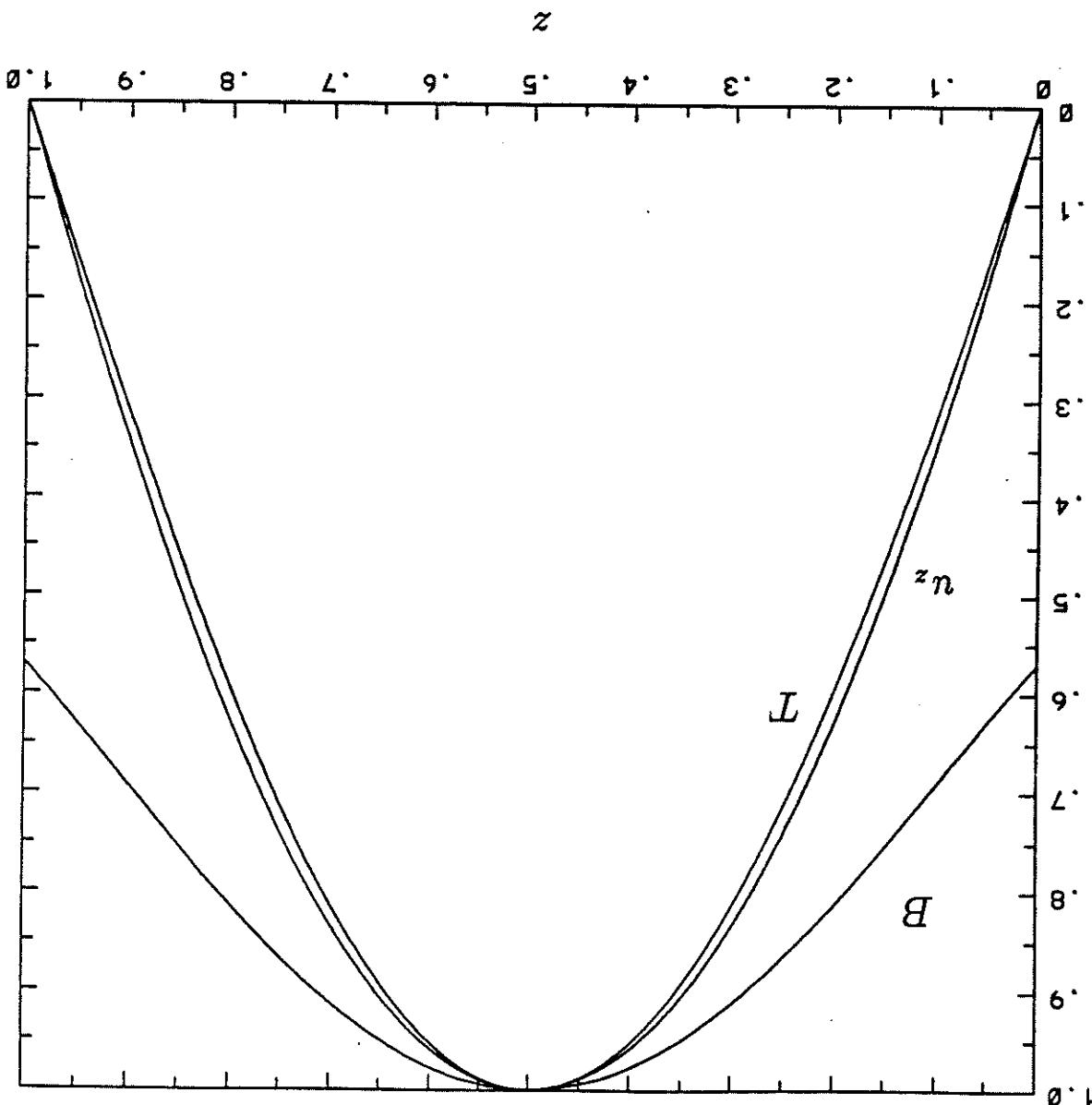


Figure 2(b). The amplitudes  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$  for the rigid duct in the case  $A = 6$  and  $r = 50$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $\tau$  on linear Boussinesq theory. Here  $a_{\max} = 3.055$ ,  $B_{\max} = 0.3508$  and  $\gamma_{\max} = 11.186$ .



Boussinesq theory.

Figure 2(c). The phases  $\theta$ ,  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$  for the rigid duct in the case  $A = 6$  and  $r = 50$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear

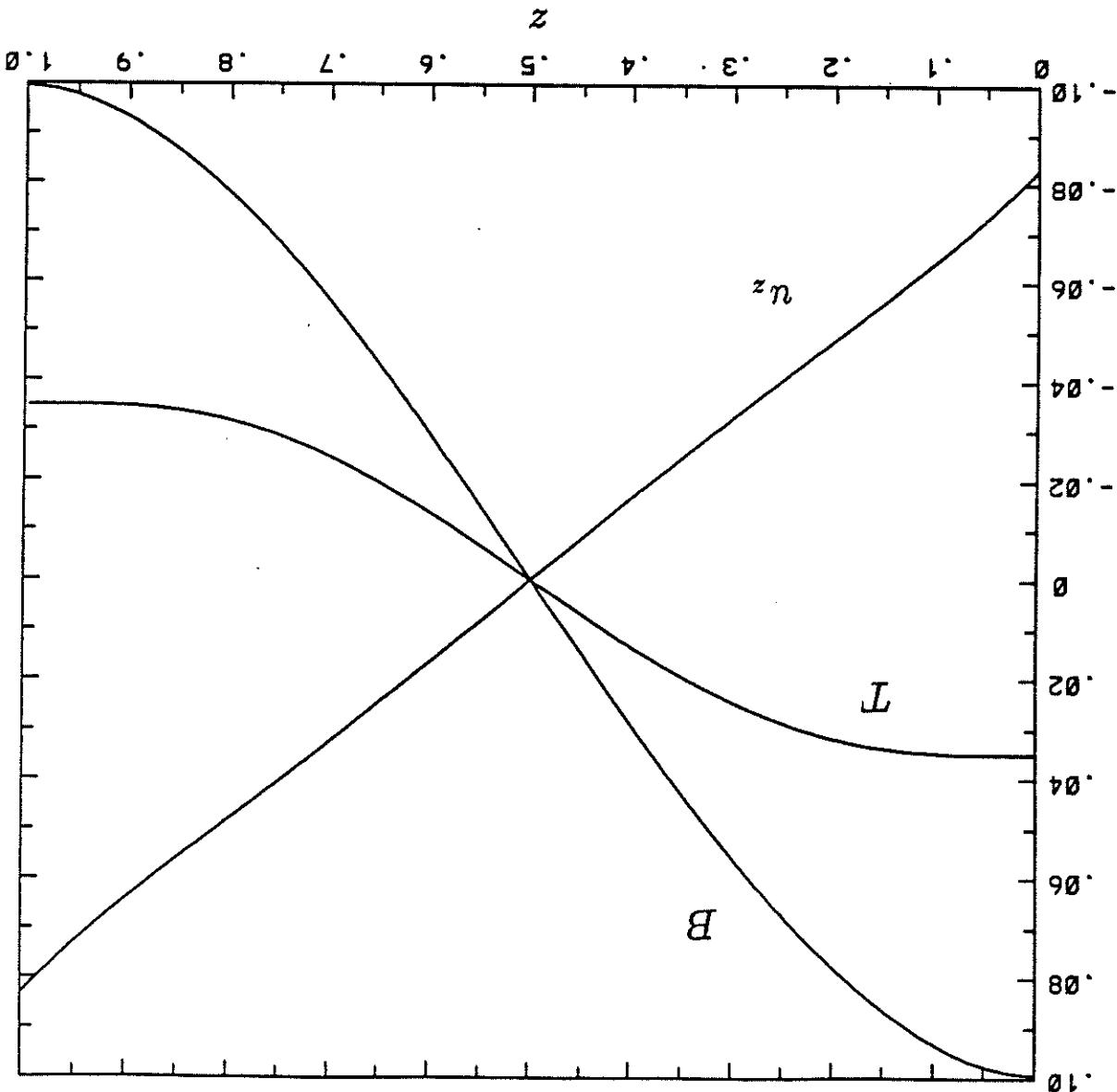


Figure 3(a). The geostrophic velocity for the rigid duct in the case  $A = 6$  and  $r = 576,503$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Here  $z$  and  $U$  are scaled as in (5.2).

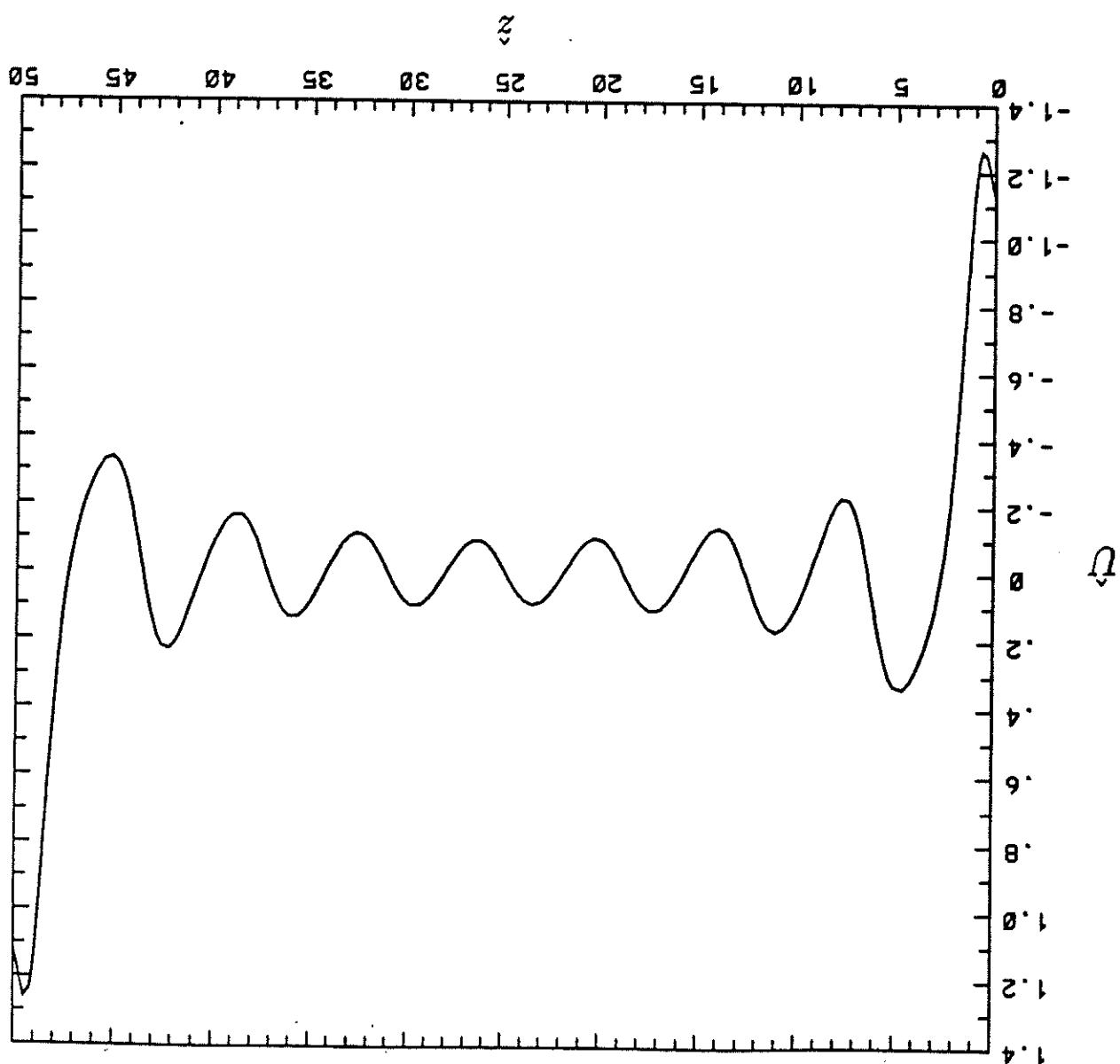
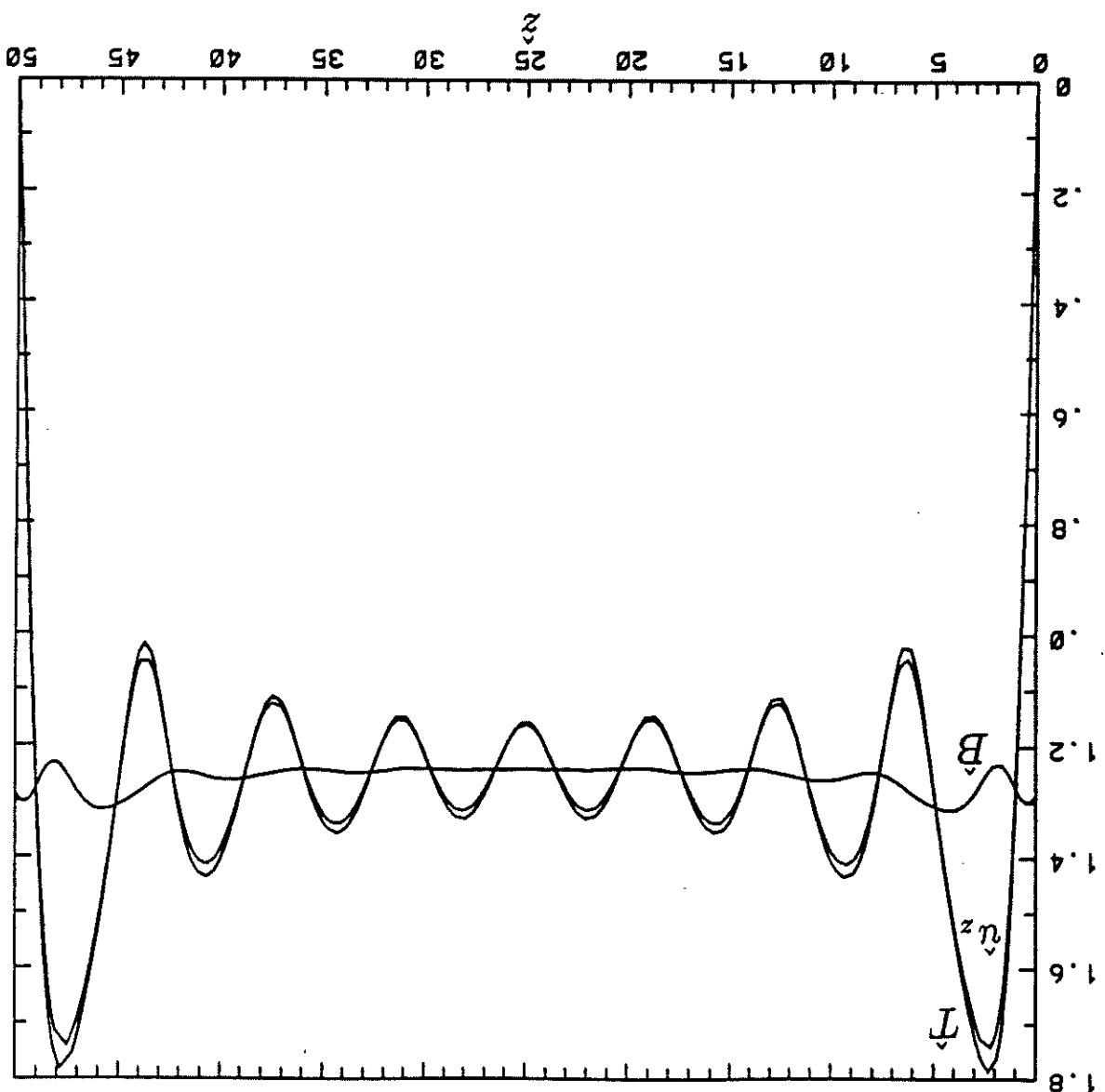


Figure 3(b). The amplitudes  $a$ ,  $B$  and  $T$  for the rigid duct in the case of linear Boussinesq theory. Here  $a$ ,  $B$  and  $T$  are scaled as in (5.2).  $A = 6$  and  $r = 576,503$  and the wavenumbers  $k = 1.117$  and  $\ell = 1.668$  that minimize  $\sigma$  on linear Boussinesq theory. Here  $a$ ,  $B$  and  $T$  are scaled as in (5.2).



Boussinesq theory. The phase of  $u_z$  is too close to that of  $T$  to be shown.  
 Figure 3(c). The phases  $\phi$  and  $\psi$  of  $B$ , and  $T$ , for the rigid duct in the case  $A = 6$  and  
 $r = 576,503$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear

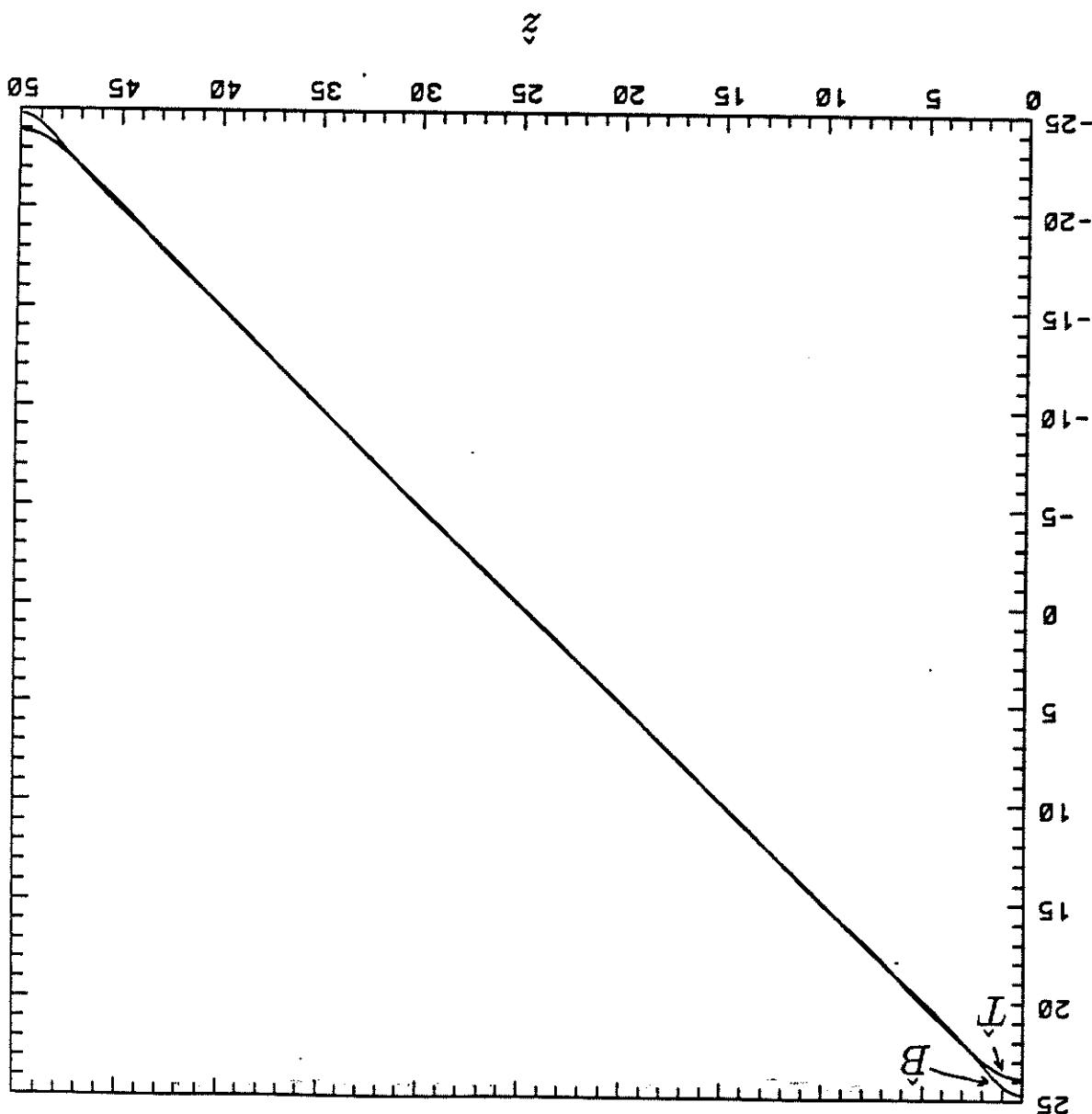


Figure 4. Bifurcation diagram for the free duct ( $A = 6$ ), showing the symmetry-breaking bifurcation,  $B_3$ . Also shown in this (r, a) plot are the marginal states of the first two modes that arise on linear Boussinesq theory for  $k = 1.117$  and  $l = 1.668$ , and also the saddle-node bifurcation,  $B_4$ .

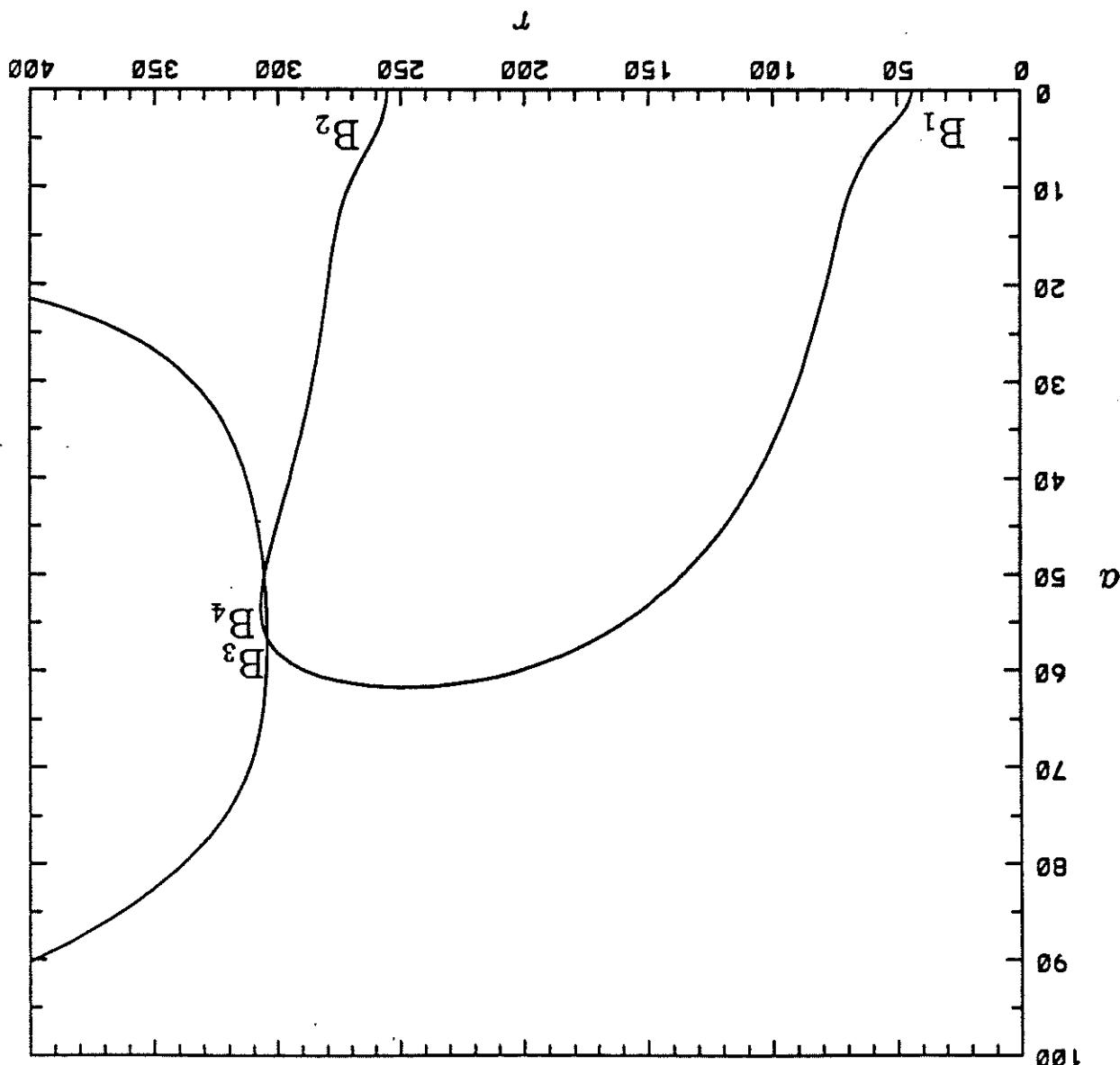
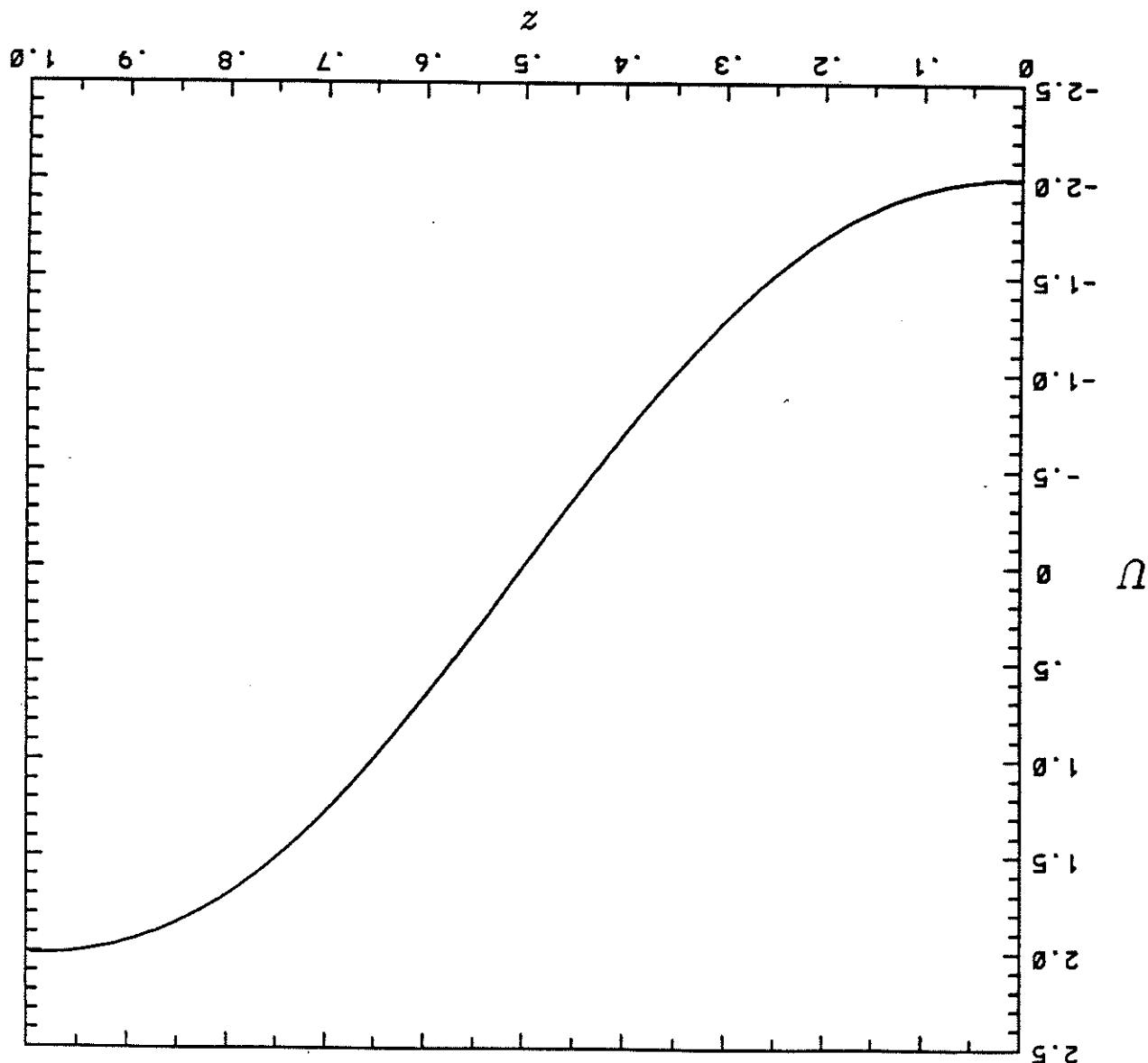


Figure 5(a). The geostrophic velocity for the free duct in the case  $A = 6$  and  $r = 50$  and the wavenumbers  $k_x = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Since  $r < r_g$ , the solution possesses the expected  $z \leftrightarrow 1 - z$  symmetry.



$\gamma_{\max} = 35.947$ . Since  $r < r_3$ , the solutions possess the expected  $z \leftrightarrow 1 - z$  symmetry. That minimizes  $\tau$  on linear Boussinesq theory. Here  $a_{\max} = 9.928$ ,  $B_{\max} = 1.123$  and  $\alpha_{\max} = 1.117$  and  $l = 1.168$  duct in the case  $A = 6$  and  $r = 50$  and the wavenumbers  $k = 1.117$  and  $l = 1.168$  Figure 5(b). The amplitudes  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$  for the three

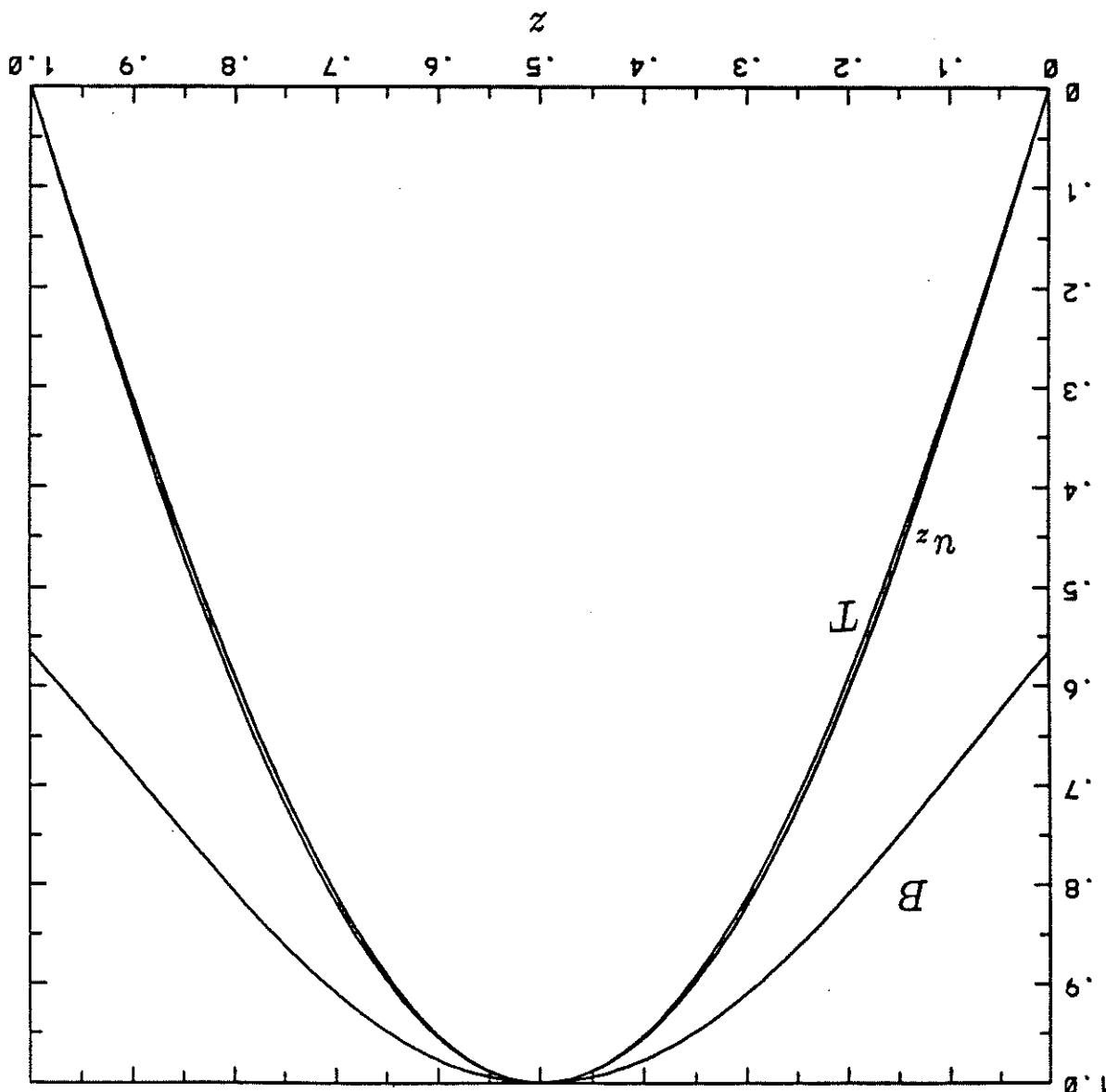


Figure 5(c). The phases  $\theta$ ,  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$  for the free duct in the case  $A = 6$  and  $r = 50$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Since  $r < r_3$ , the solutions possess the expected  $z \leftrightarrow 1 - z$  symmetry.

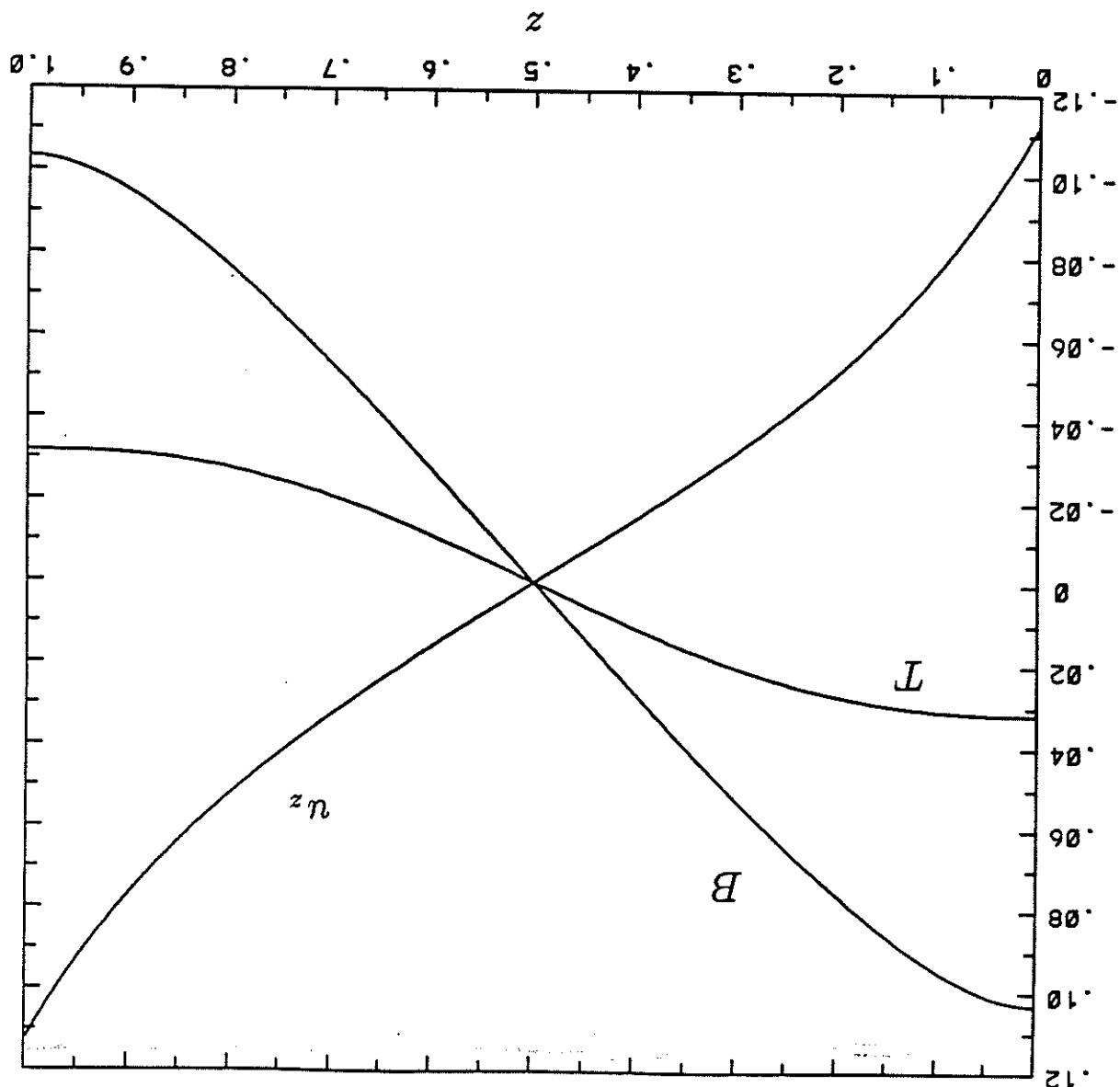


Figure 6(a). The geostrophic velocity for the free duct in the case  $A = 6$  and  $r = 320 > r_3$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Since  $r > r_3$ , the solution does not possess  $z \leftrightarrow 1 - z$  symmetry.

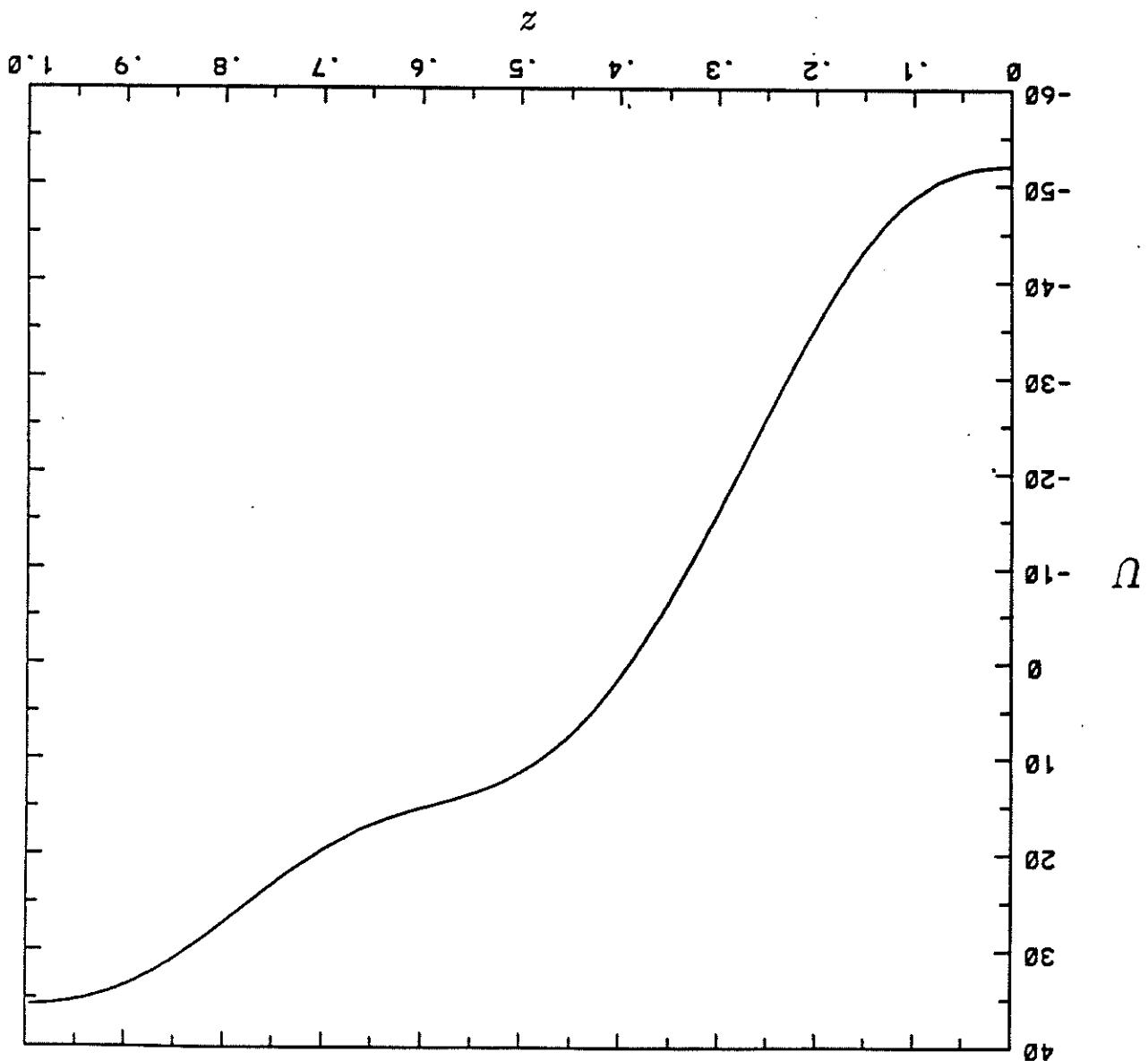


Figure 6(b). The amplitudes  $a/a_{\max}$ ,  $b/b_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$  for the free duct  $\gamma_{\max} = 1126.5$ . Since  $r > r_3$ , the solutions do not possess  $z \leftrightarrow 1 - z$  symmetry. In the case  $A = 6$  and  $r = 320 > r_3$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Here  $a_{\max} = 153.42$ ,  $b_{\max} = 3.365$  and  $\gamma_{\max} = 1126.5$ .

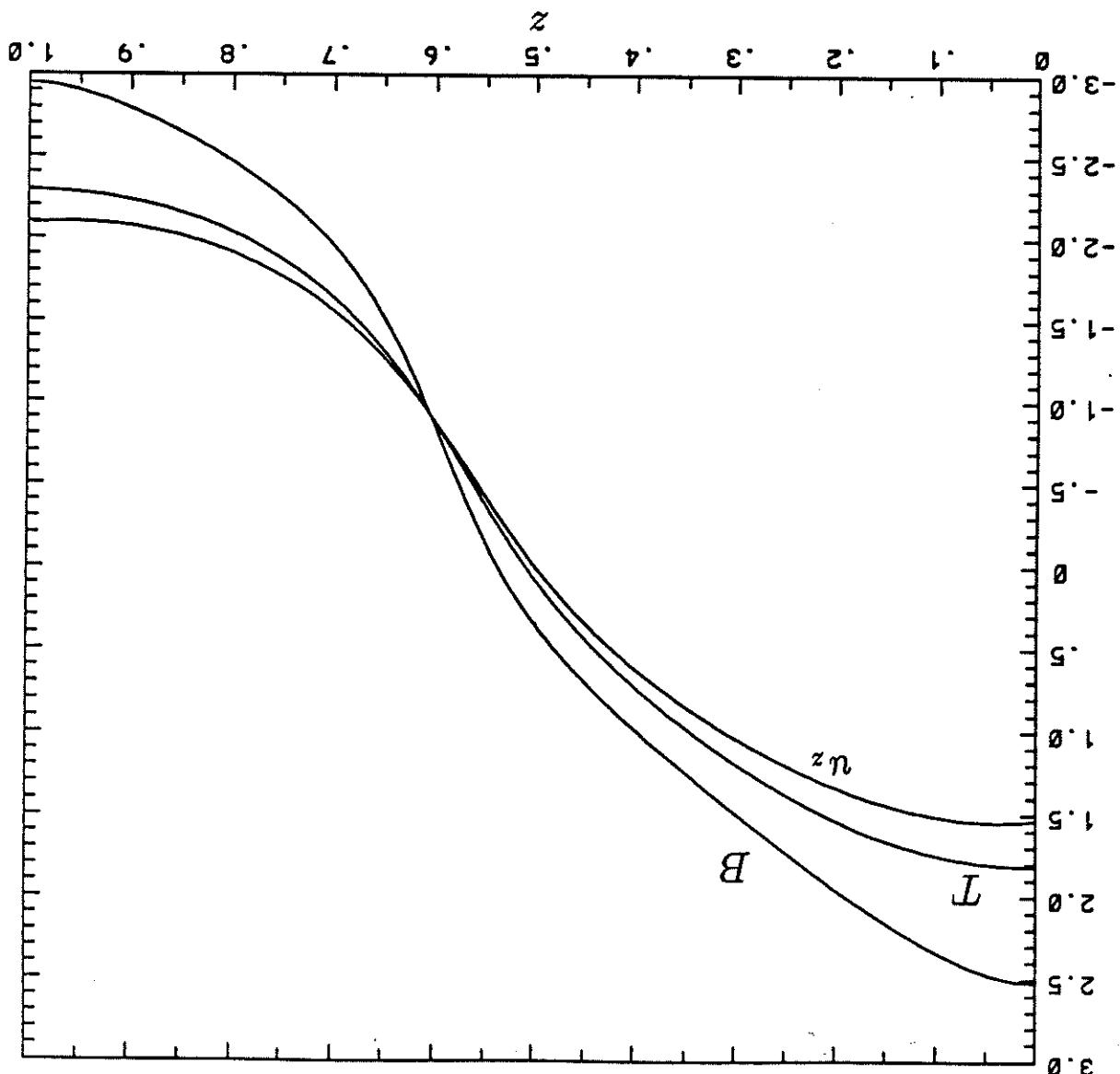


Figure 6(c). The phases  $\theta$ ,  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$  for the free duct in the case  $A = 6$  and  $r = 320 > r_3$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Since  $r > r_3$ , the solutions do not possess  $z \leftrightarrow l - z$  symmetry.

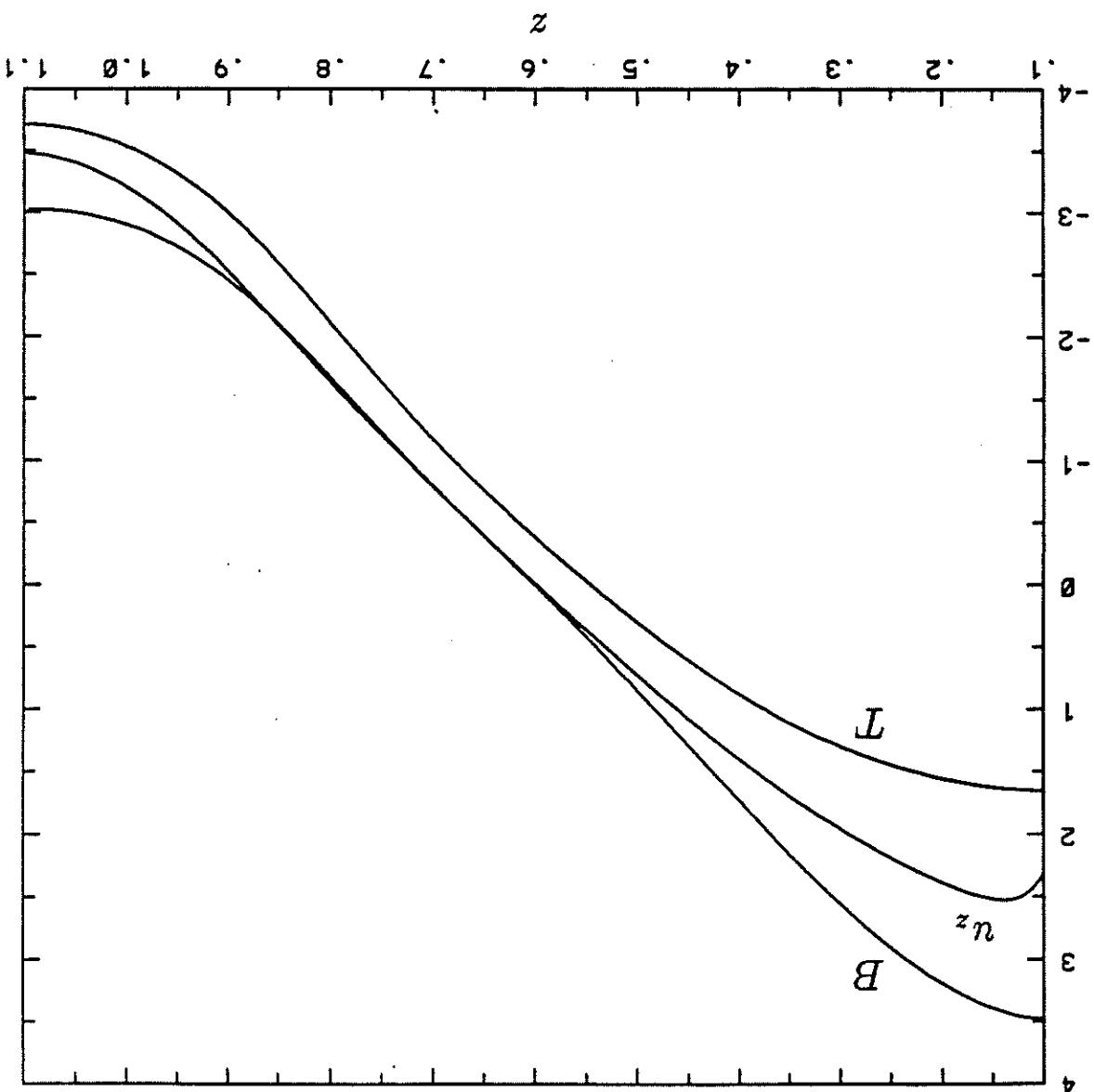


Figure 7(a). The geostrophic velocity for the free duct in the case  $A = 6$  and  $r = 576,503$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. Here  $z$  and  $U$ , are scaled as in (6.2).

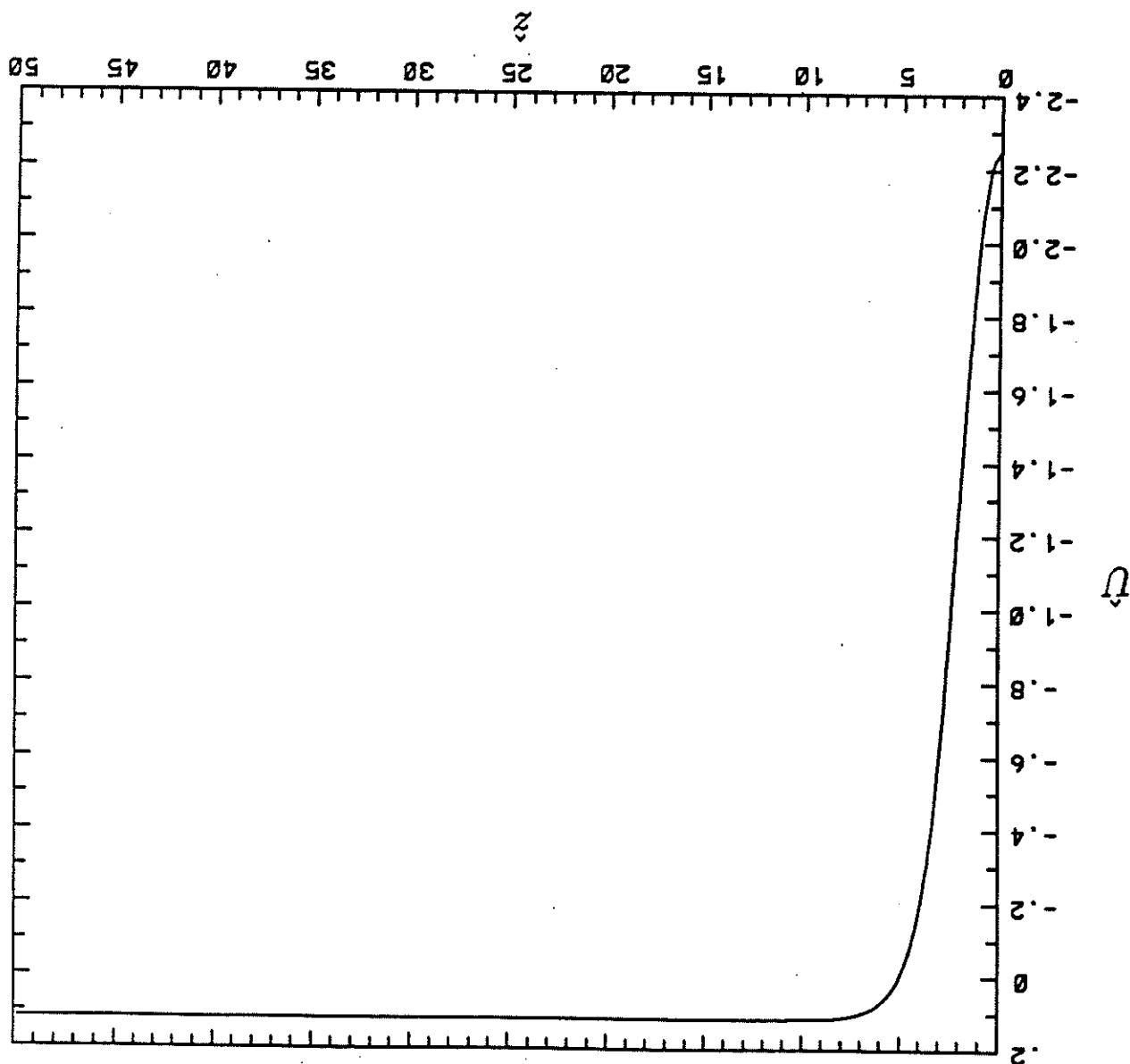


Figure 7(b). The amplitudes  $a$ ,  $B$  and  $\gamma$  of  $u_z$ ,  $B$ , and  $T$  for the free duct in the case of linear Boussinesq theory. Here  $z$ ,  $a$ ,  $B$  and  $\gamma$  are scaled as in (6.2).

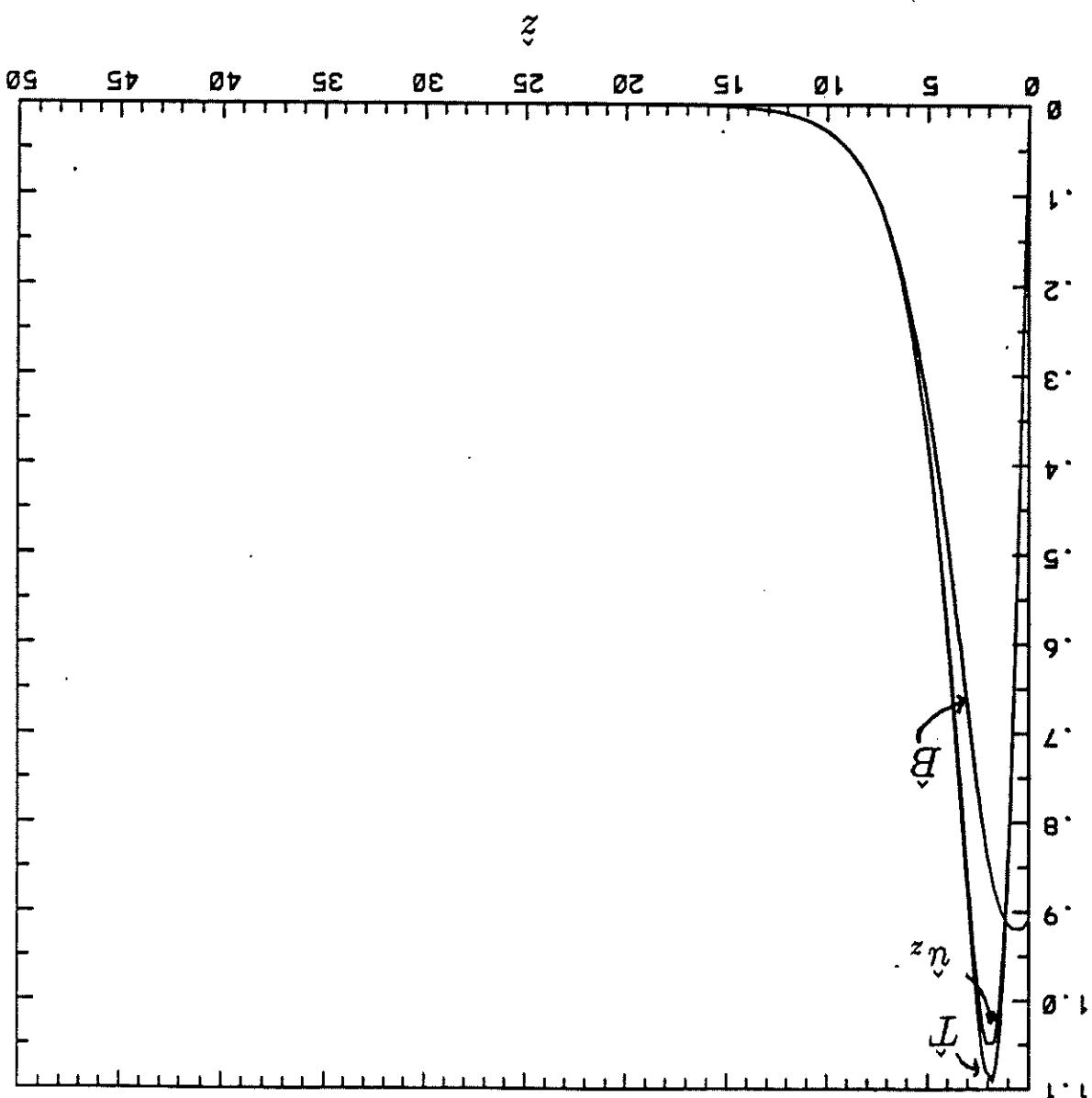


Figure 7(c). The phases  $\phi$  and  $\psi$  of  $B$ , and  $T$  for the free duct in the case  $A = 6$  and  $r = 576, 503$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory. The phase of  $u_z$  is too close to that of  $T$  to be shown in (c).

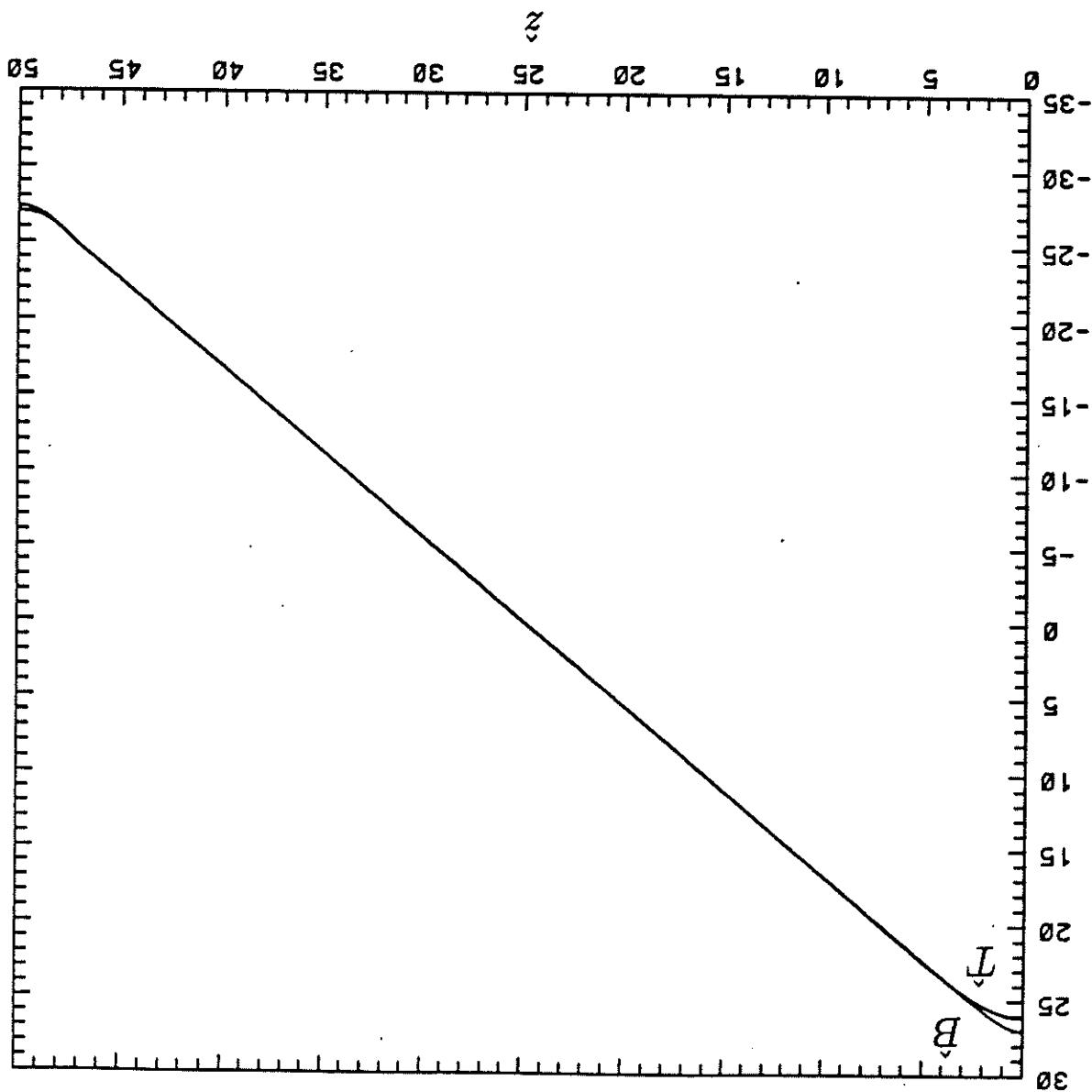
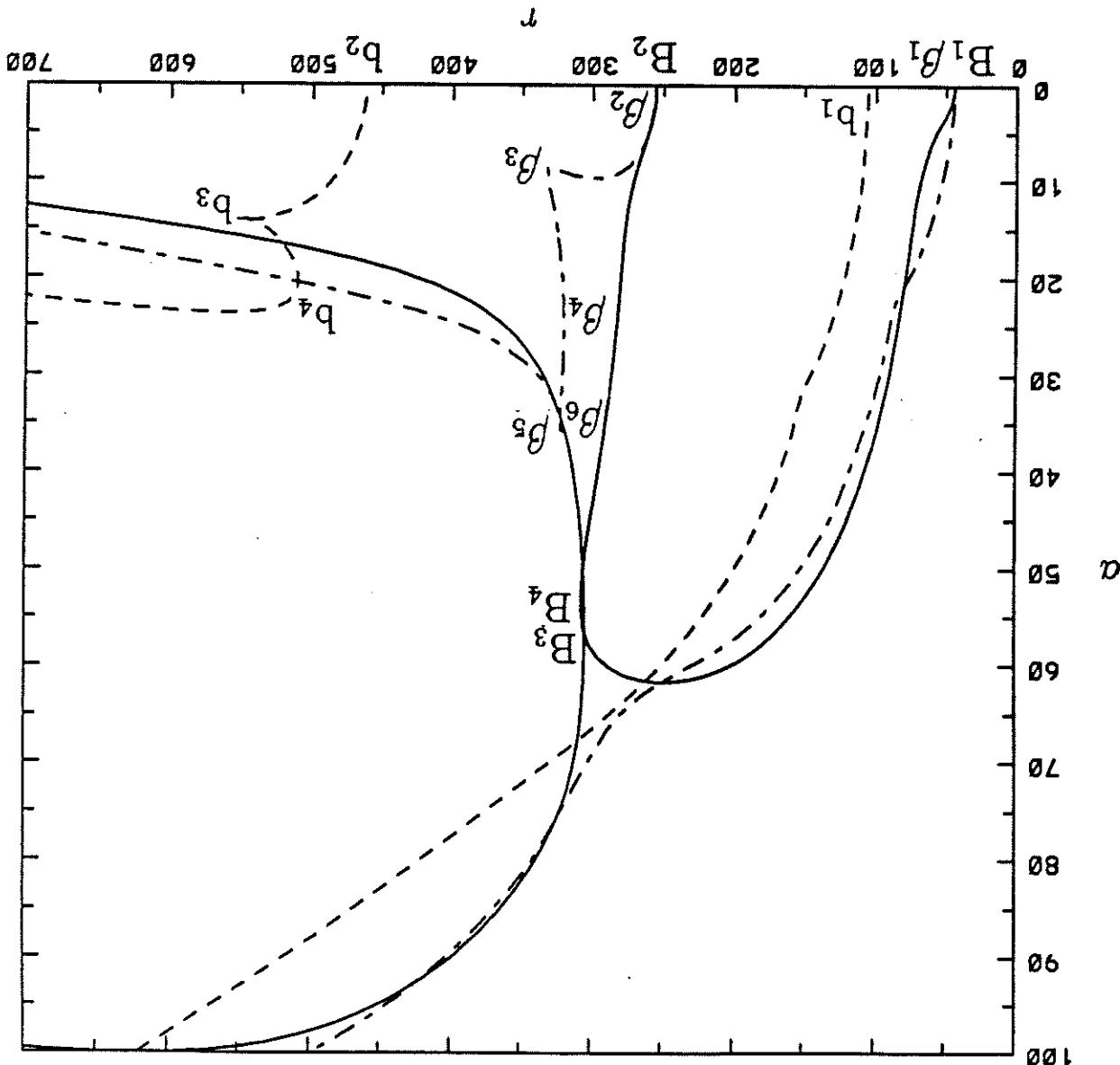


Figure 8. Bifurcation diagrams for the free compressible duct in three cases:



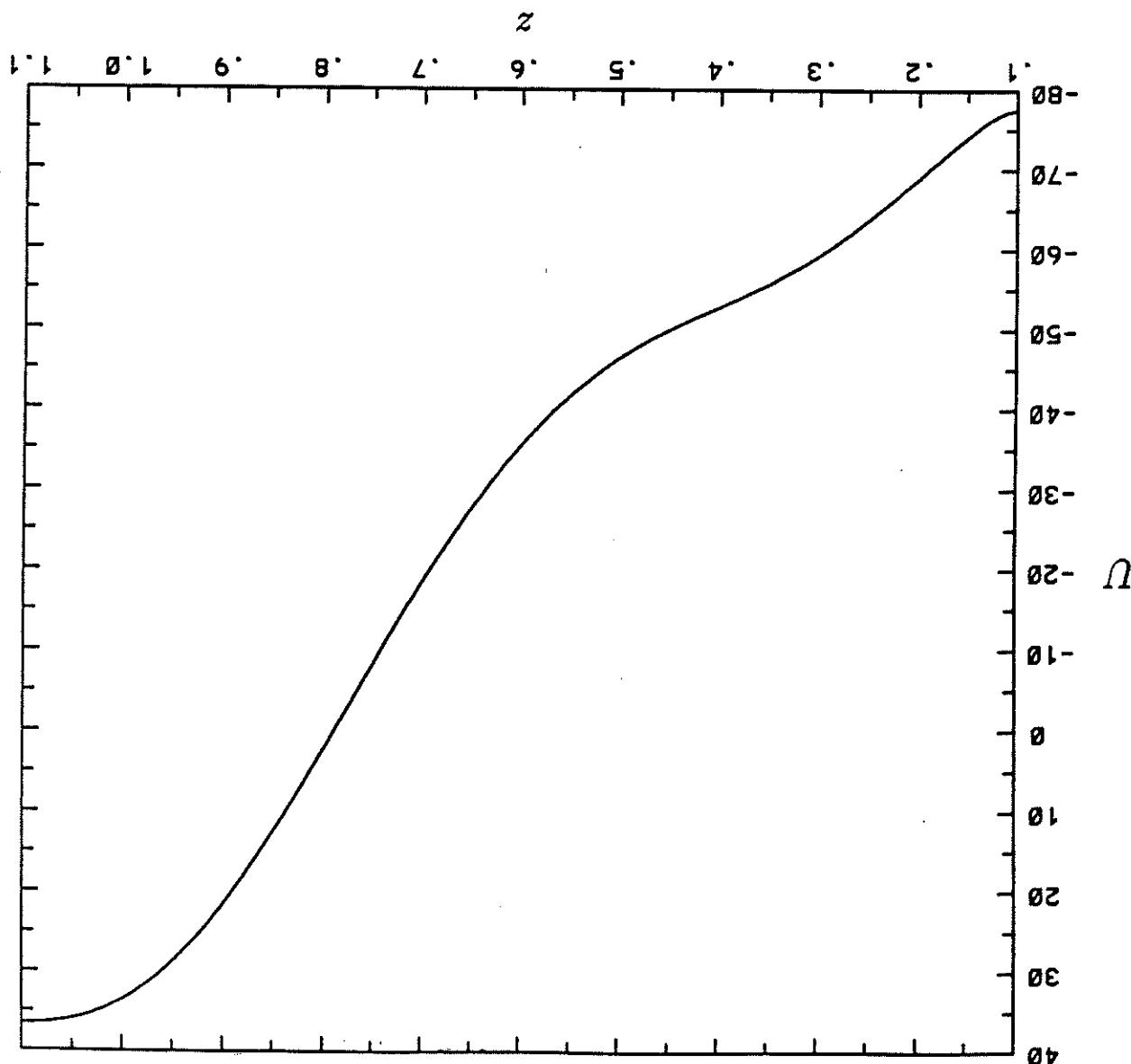
The unfolding of the symmetry-breaking bifurcation,  $B_3$ , of (a) as  $z_0$  is decreased is evident.

(c) a highly compressible case ( $z_0 = 0.1$ );

(b) a slightly compressible case ( $z_0 = 1.0$ );

(a) the Boussinesq limit ( $z_0 \rightarrow \infty$ );

Figure 9(a). The geostrophic velocity on the primary branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory for  $A = 6$ .



Theory for  $A = 6$ . Here  $a_{\max} = 373.07$ ,  $B_{\max} = 2.911$  and  $\gamma_{\max} = 2848.0$   
 and the wavenumbers  $k = 1.117$  and  $\ell = 1.668$  that minimize  $r$  on linear Boussinesq  
 branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$   
 Figure 9(b). The amplitudes  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$  on the primary

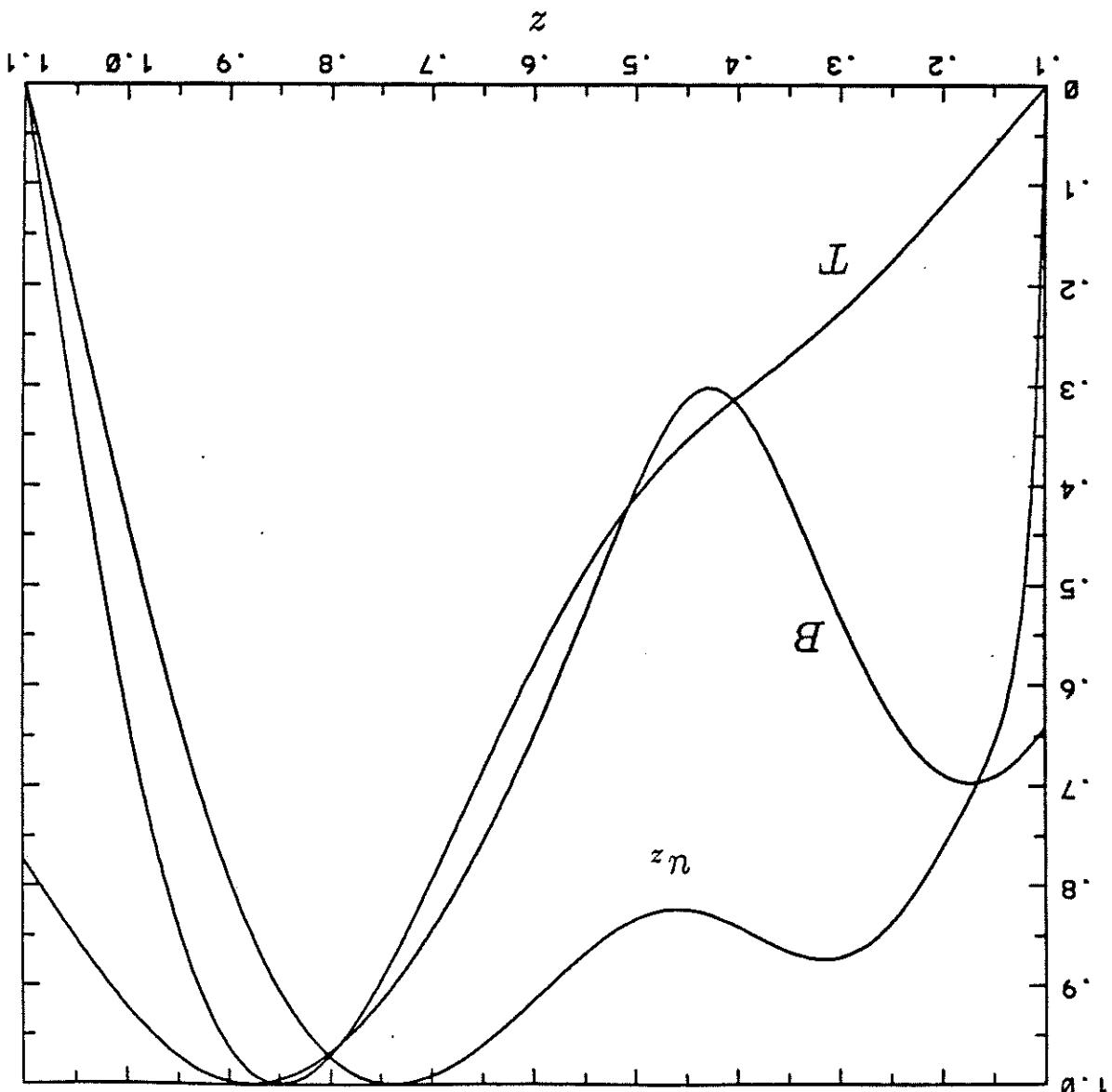
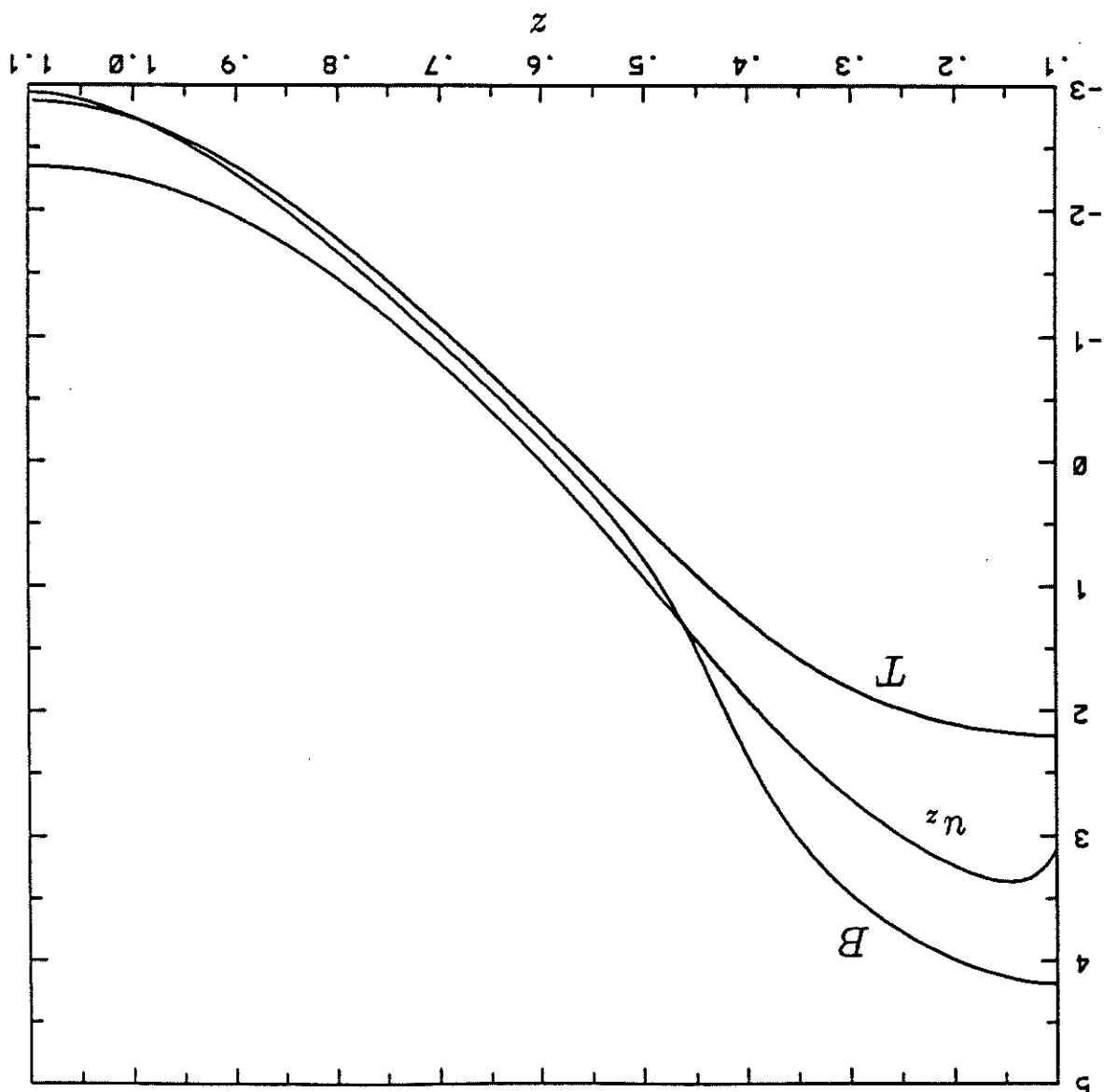


Figure 9(c). The phases  $\theta$ ,  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$  on the primary branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory for  $A = 6$ .



$k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory.  
 compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  
 Figure 10(a). The geostrophic velocity on the secondary branch for convection in the free

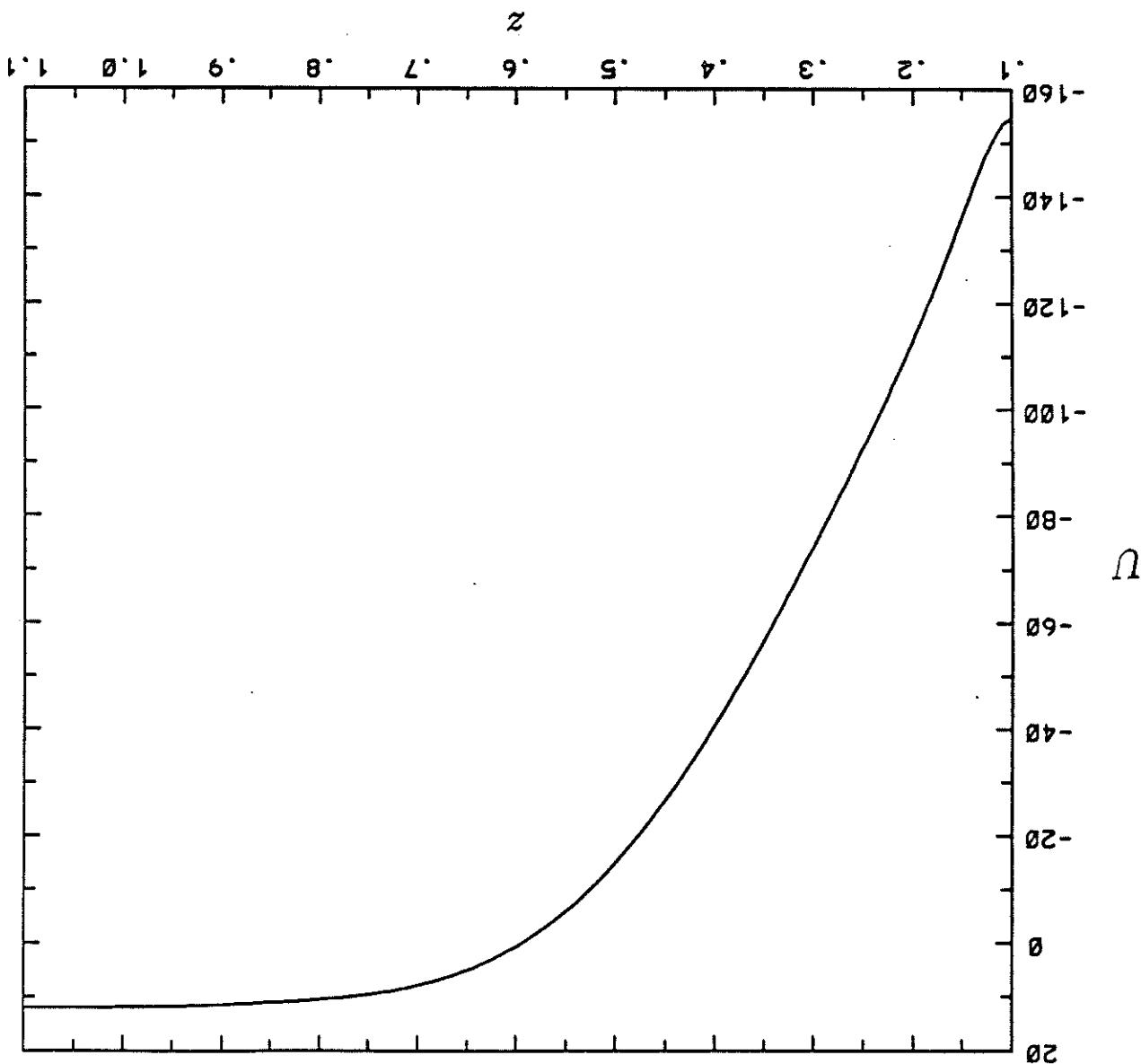


Figure 10(b). The amplitudes  $a/a_{\max}$ ,  $B/B_{\max}$  and  $\gamma/\gamma_{\max}$  of  $u_z$ ,  $B$ , and  $T$  on the secondary branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  $k = 1.117$  and  $\ell = 1.668$  that minimize  $r$  on linear Boussinesq theory. Here  $a_{\max} = 673.42$ ,  $B_{\max} = 4.358$  and  $\gamma_{\max} = 1690.5$ .

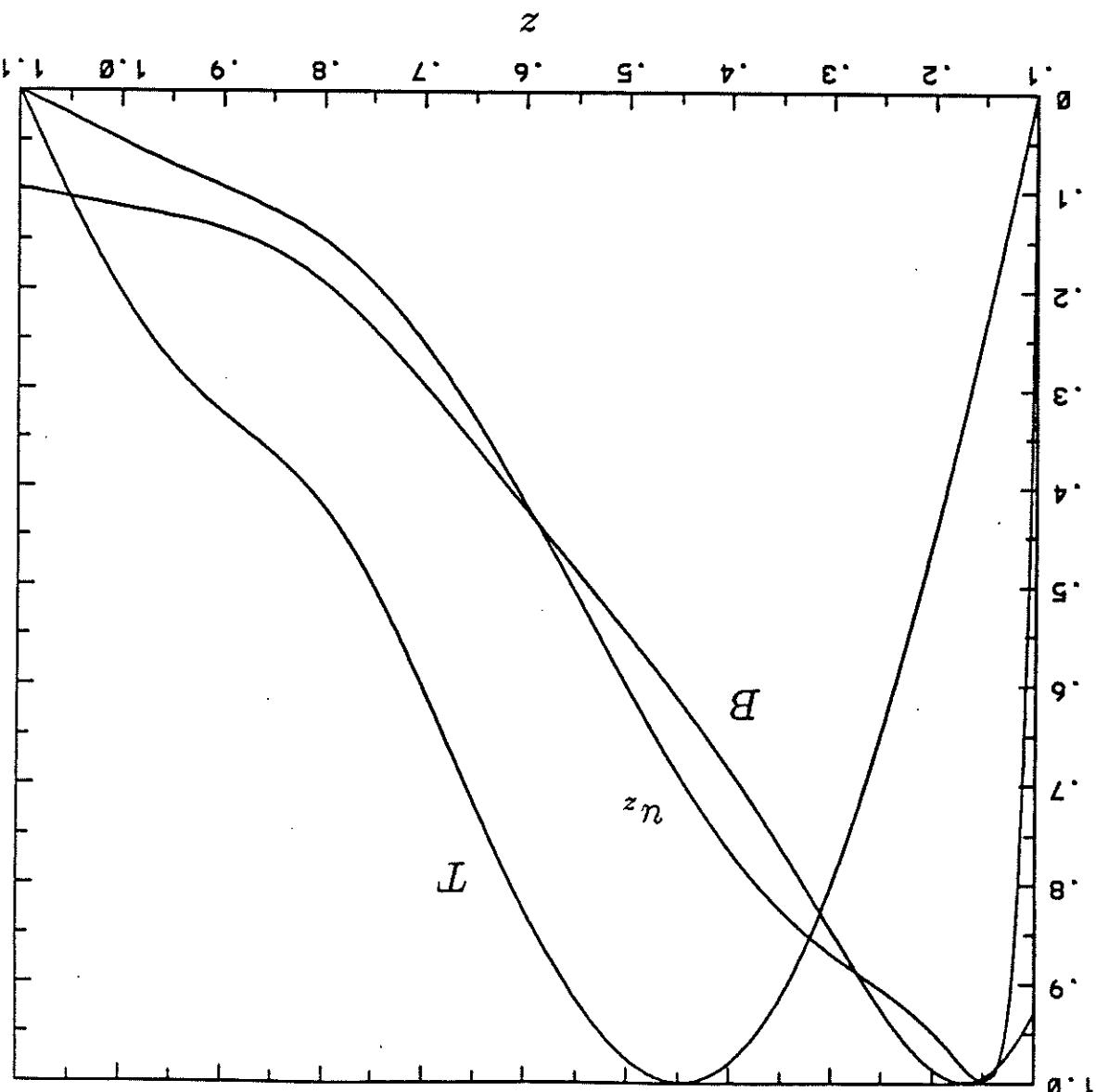


Figure 10(c). The phases  $\theta$ ,  $\phi$  and  $\psi$  of  $u_z$ ,  $B$ , and  $T$  on the secondary branch for convection in the free compressible duct for the case  $z_0 = 0.1$ ,  $A = 6$ ,  $r = 700$  and the wavenumbers  $k = 1.117$  and  $l = 1.668$  that minimize  $r$  on linear Boussinesq theory.

